

# SCY99194

## Fixed Frequency Current Mode Controller for Flyback Converters

The SCY99194 is a new fixed-frequency current-mode controller featuring the Dynamic Self-Supply. This function greatly simplifies the design of the auxiliary supply and the  $V_{CC}$  capacitor by activating the internal startup current source to supply the controller during start-up, transients, latch, stand-by etc. This device contains a special HV detector which detect the application unplug from the AC input line and triggers the X2 discharge current.

It features a timer-based fault detection that ensures the detection of overload and an adjustable compensation to help keep the maximum power independent of the input voltage.

Due to frequency foldback, the controller exhibits excellent efficiency in light load condition while still achieving very low standby power consumption. Internal frequency jittering, ramp compensation, and a versatile latch input make this controller an excellent candidate for the robust power supply designs.

A dedicated Off mode allows to reach the extremely low no load input power consumption via “sleeping” whole device and thus minimize the power consumption of the control circuitry.

### Features

- Fixed-Frequency Current-Mode Operation (65 kHz Switching Frequency)
- Frequency Foldback then Skip Mode for Maximized Performance in Light Load and Standby Conditions
- Timer-Based Overload Protection with Latched (Option A) or Auto-Recovery (Option B) Operation
- High-voltage Current Source with Dynamic Self-Supply, Simplifying the Design of the  $V_{CC}$  Circuitry
- Frequency Modulation for Softened EMI Signature
- Adjustable Overpower Protection Dependant on the Bulk Voltage
- Latch-off Input Combined with the Overpower Protection Sensing Input
- $V_{CC}$  Operation up to 28 V, With Overvoltage Detection
- 500/800 mA Source/Sink Drive Peak Current Capability
- 10 ms Soft-Start
- Internal Thermal Shutdown
- No-Load Standby Power < 30 mW
- X2 Capacitor in EMI Filter Discharging Feature
- These Devices are Pb-Free and Halogen Free/BFR Free

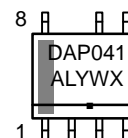


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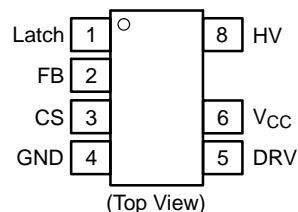
### MARKING DIAGRAM

  
SOIC-7  
CASE 751U



DAP041 = Specific Device Code  
A = Assembly Location  
L = Wafer Lot  
Y = Year  
W = Work Week  
▪ = Pb-Free Package

### PIN CONNECTIONS



### ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page 39 of this data sheet.

### Typical Applications

- AC-DC Adapters for Notebooks, LCD, and Printers
- Offline Battery Chargers
- Consumer Electronic Power Supplies
- Auxiliary/Housekeeping Power Supplies
- Offline Adapters for Notebooks

# SCY99194

## TYPICAL APPLICATION EXAMPLE

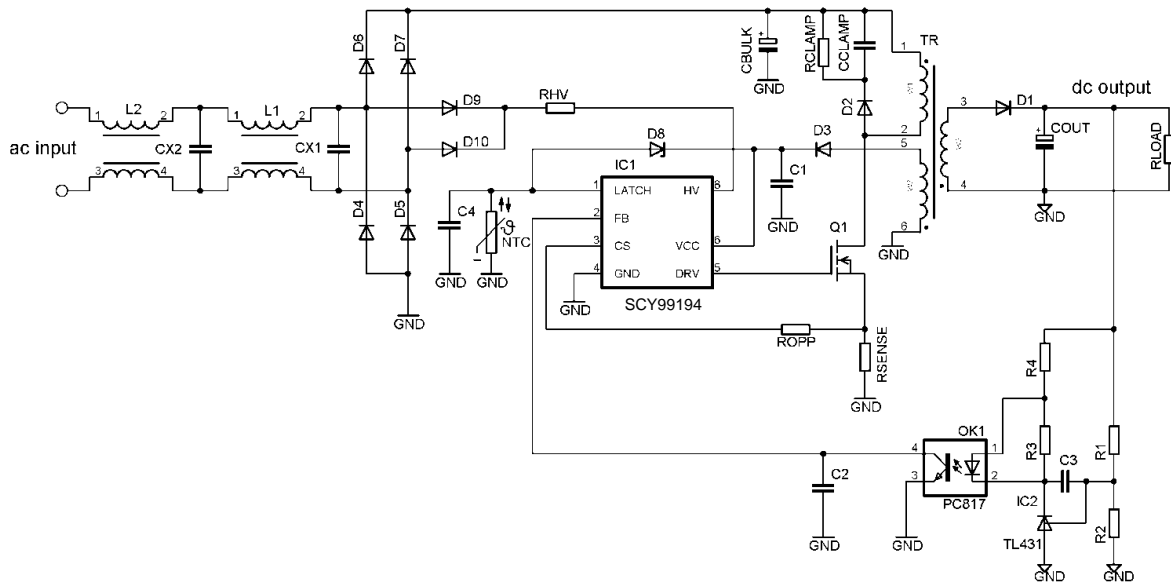


Figure 1. Flyback Converter Application Using the SCY99194

### PIN FUNCTION DESCRIPTION

Pin No	Pin Name	Function	Pin Description
1	LATCH	Latch-Off Input	Pull the pin up or down to latch-off the controller. An internal current source allows the direct connection of an NTC for over temperature detection.
2	FB	Feedback + Shutdown pin	An optocoupler collector to ground controls the output regulation. The part goes to the low consumption Off mode if the FB input pin is pulled to GND.
3	CS	Current Sense	This Input senses the Primary Current for current-mode operation, and offers an overpower compensation adjustment.
4	GND	-	The controller ground
5	DRV	Drive output	Drives external MOSFET
6	VCC	VCC input	This supply pin accepts up to 28 Vdc, with overvoltage detection. The pin is connected to an external auxiliary voltage. It is not allowed to connect another circuit to this pin to keep low input power consumption.
8	HV	High-voltage pin	Connects to the rectified AC line to perform the functions of Start-up Current Source, Self-Supply and X2 capacitor discharge function and the HV sensing for the overpower protection purposes. It is not allowed to connect this pin to DC voltage.

SIMPLIFIED INTERNAL BLOCK SCHEMATIC

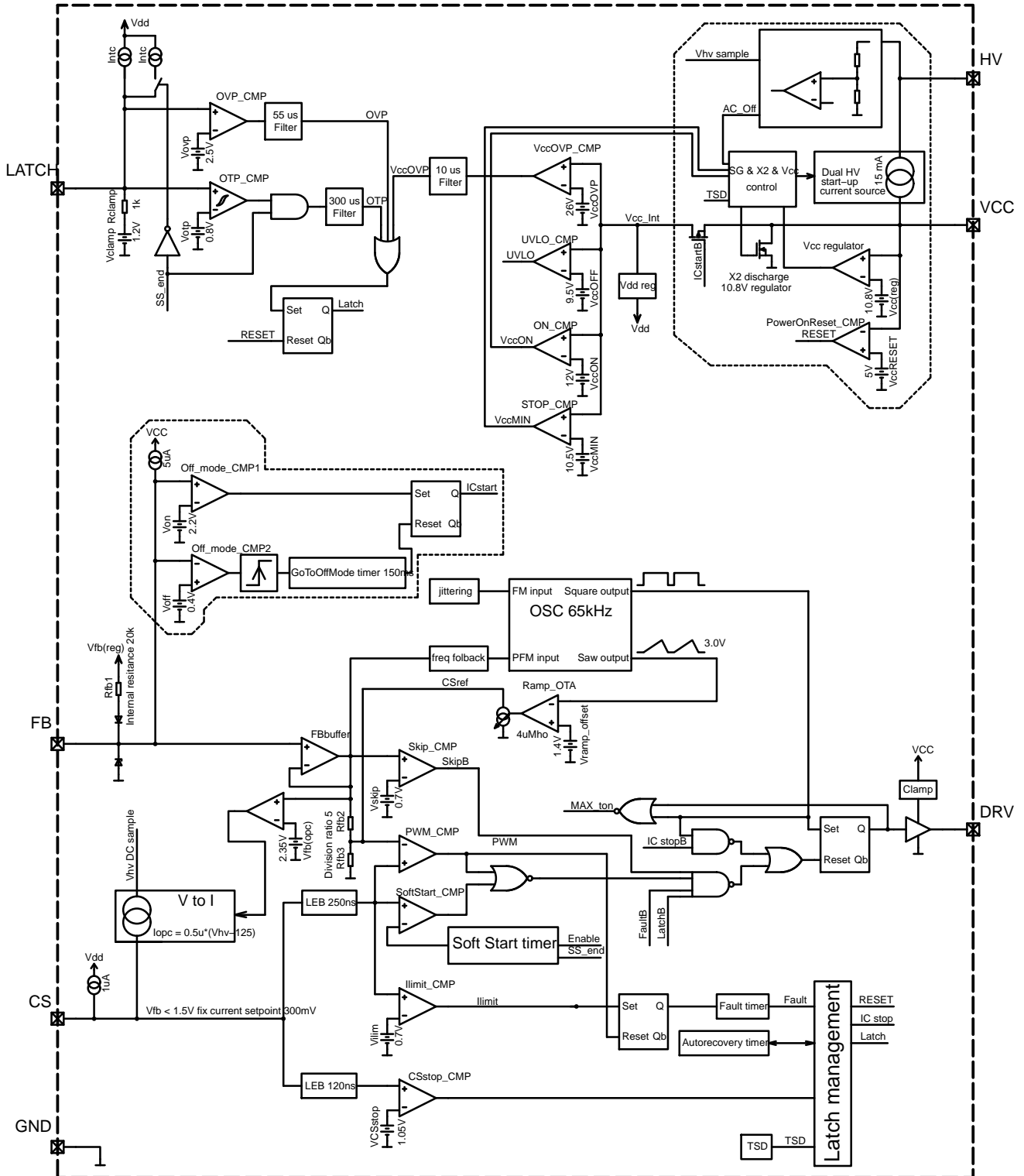


Figure 2. Simplified Internal Block Schematic

# SCY99194

## MAXIMUM RATINGS

Rating	Symbol	Value	Unit
DRV (pin 5)	Maximum voltage on DRV pin (Dc-Current self-limited if operated within the allowed range) (Note 1)	-0.3 to 20 ±1000 (peak)	V mA
V <sub>CC</sub> (pin 6)	V <sub>CC</sub> Power Supply voltage, V <sub>CC</sub> pin, continuous voltage Power Supply voltage, V <sub>CC</sub> pin, continuous voltage (Note 1)	-0.3 to 28 ±30 (peak)	V mA
HV (pin 8)	Maximum voltage on HV pin (Dc-Current self-limited if operated within the allowed range)	-0.3 to 500 ±20	V mA
V <sub>max</sub>	Maximum voltage on low power pins (except pin 5, pin 6 and pin 8) (Dc-Current self-limited if operated within the allowed range) (Note 1)	-0.3 to 10 ±10 (peak)	V mA
R <sub>θJ-A</sub>	Thermal Resistance SOIC-7 Junction-to-Air, low conductivity PCB (Note 2) Junction-to-Air, medium conductivity PCB (Note 3) Junction-to-Air, high conductivity PCB (Note 4)	162 147 115	°C/W
R <sub>θJ-C</sub>	Thermal Resistance Junction-to-Case	73	°C/W
T <sub>JMAX</sub>	Operating Junction Temperature	-40 to +150	°C
T <sub>STRGMAX</sub>	Storage Temperature Range	-60 to +150	°C
	ESD Capability, HBM model (All pins except HV) per JEDEC Standard JESD22, Method A114E	> 2000	V
	ESD Capability, Machine Model per JEDEC Standard JESD22, Method A115A	> 200	V
	ESD Capability, Charged Device Model per JEDEC Standard JESD22, Method C101E	> 1000	V

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

1. This device contains latch-up protection and exceeds 100 mA per JEDEC Standard JESD78.
2. As mounted on a 80 x 100 x 1.5 mm FR4 substrate with a single layer of 50 mm<sup>2</sup> of 2 oz copper traces and heat spreading area. As specified for a JEDEC 51-1 conductivity test PCB. Test conditions were under natural convection or zero air flow.
3. As mounted on a 80 x 100 x 1.5 mm FR4 substrate with a single layer of 100 mm<sup>2</sup> of 2 oz copper traces and heat spreading area. As specified for a JEDEC 51-2 conductivity test PCB. Test conditions were under natural convection or zero air flow.
4. As mounted on a 80 x 100 x 1.5 mm FR4 substrate with a single layer of 650 mm<sup>2</sup> of 2 oz copper traces and heat spreading area. As specified for a JEDEC 51-3 conductivity test PCB. Test conditions were under natural convection or zero air flow.

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**ELECTRICAL CHARACTERISTICS** (For typical values  $T_J = 25^\circ\text{C}$ , for min/max values  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ ,  $V_{HV} = 125\text{ V}$ ,  $V_{CC} = 11\text{ V}$  unless otherwise noted)

Characteristics	Test Condition	Symbol	Min	Typ	Max	Unit
<b>HIGH VOLTAGE CURRENT SOURCE</b>						
Minimum voltage for current source operation		$V_{HV(\text{min})}$	–	30	40	V
Current flowing out of $V_{CC}$ pin	$V_{CC} = 0\text{ V}$ $V_{CC} = V_{CC(\text{on})} - 0.5\text{ V}$	$I_{\text{start1}}$ $I_{\text{start2}}$	0.2 5	0.5 8	0.8 11	mA
Off-state leakage current	$V_{HV} = 500\text{ V}$ , $V_{CC} = 15\text{ V}$	$I_{\text{start(off)}}$	10	25	50	$\mu\text{A}$
Off-mode HV supply current	$V_{HV} = 141\text{ V}$ , $V_{HV} = 325\text{ V}$ , $V_{CC}$ loaded by $4.7\ \mu\text{F}$ cap	$I_{HV(\text{off})}$	– –	45 50	60 70	$\mu\text{A}$

## SUPPLY

HV current source regulation threshold		$V_{CC(\text{reg})}$	8	11	–	V
Turn-on threshold level, $V_{CC}$ going up HV current source stop threshold		$V_{CC(\text{on})}$	11.0	12.0	13.0	V
HV current source restart threshold		$V_{CC(\text{min})}$	9.5	10.5	11.5	V
Turn-off threshold		$V_{CC(\text{off})}$	8.5	8.9	9.3	V
Overvoltage threshold		$V_{CC(\text{ovp})}$	25	26.5	28	V
Blanking duration on $V_{CC(\text{off})}$ and $V_{CC(\text{ovp})}$ detection		$t_{VCC(\text{blank})}$	–	10	–	$\mu\text{s}$
$V_{CC}$ decreasing level at which the internal logic resets		$V_{CC(\text{reset})}$	4.8	7.0	7.7	V
$V_{CC}$ level for $I_{\text{START1}}$ to $I_{\text{START2}}$ transition		$V_{CC(\text{inhibit})}$	0.2	0.8	1.25	V
Internal current consumption (Note 5)	DRV open, $V_{FB} = 3\text{ V}$ , 65 kHz	$I_{CC1}$	1.3	1.85	2.2	mA
	Cdrv = 1 nF, $V_{FB} = 3\text{ V}$ , 65 kHz	$I_{CC2}$	1.8	2.6	3.0	
	Off mode (skip or before start-up)	$I_{CC3}$	0.67	0.9	1.13	
	Fault mode (fault or latch)	$I_{CC4}$	0.3	0.6	0.9	

## X2 DISCHARGE

Comparator hysteresis observed at HV pin		$V_{HV(\text{hyst})}$	1.5	3.5	5	V
HV signal sampling period		$T_{\text{sample}}$	–	1.0	–	ms
Timer duration for no line detection		$t_{\text{DET}}$	21	32	43	ms
Discharge timer duration		$t_{\text{DIS}}$	21	32	43	ms

## OSCILLATOR

Oscillator frequency		$f_{\text{OSC}}$	58	65	72	kHz
Maximum duty cycle		$D_{\text{MAX}}$	–	80	–	%
Frequency jittering amplitude, in percentage of $F_{\text{OSC}}$		$A_{\text{jitter}}$	$\pm 4$	$\pm 6$	$\pm 8$	%
Frequency jittering modulation frequency		$F_{\text{jitter}}$	85	125	165	Hz

## FREQUENCY FOLDBACK

Feedback voltage threshold below which frequency foldback starts		$V_{FB(\text{foldS})}$	1.8	2.0	2.2	V
Feedback voltage threshold below which frequency foldback is complete		$V_{FB(\text{foldE})}$	0.8	0.9	1.0	V
Minimum switching frequency	$V_{FB} = V_{\text{skip(in)}} + 0.1$	$f_{\text{OSC(min)}}$	22	27	32	kHz

5. Internal supply current only, currents sourced via FB pin is not included (current is flowing in GND pin only).

6. Guaranteed by design.

7. CS pin source current is a sum of  $I_{\text{bias}}$  and  $I_{\text{OPC}}$ , thus at  $V_{HV} = 125\text{ V}$  is observed the  $I_{\text{bias}}$  only, because  $I_{\text{OPC}}$  is switched off.

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**ELECTRICAL CHARACTERISTICS** (For typical values  $T_J = 25^\circ\text{C}$ , for min/max values  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ ,  $V_{HV} = 125\text{ V}$ ,  $V_{CC} = 11\text{ V}$  unless otherwise noted)

Characteristics	Test Condition	Symbol	Min	Typ	Max	Unit
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## OUTPUT DRIVER

Rise time, 10 to 90% of $V_{CC}$	$V_{CC} = V_{CC(\text{min})} + 0.2\text{ V}$ , $C_{\text{DRV}} = 1\text{ nF}$	$t_{\text{rise}}$	–	40	70	ns
Fall time, 90 to 10% of $V_{CC}$	$V_{CC} = V_{CC(\text{min})} + 0.2\text{ V}$ , $C_{\text{DRV}} = 1\text{ nF}$	$t_{\text{fall}}$	–	40	70	ns
Current capability	$V_{CC} = V_{CC(\text{min})} + 0.2\text{ V}$ , $C_{\text{DRV}} = 1\text{ nF}$ DRV high, $V_{\text{DRV}} = 0\text{ V}$ DRV low, $V_{\text{DRV}} = V_{CC}$	$I_{\text{DRV}(\text{source})}$ $I_{\text{DRV}(\text{sink})}$	– –	500 800	– –	mA
Clamping voltage (maximum gate voltage)	$V_{CC} = V_{CC(\text{max})} - 0.2\text{ V}$ , DRV high, $R_{\text{DRV}} = 33\text{ k}\Omega$ , $C_{\text{load}} = 220\text{ pF}$	$V_{\text{DRV}(\text{clamp})}$	11	13.5	16	V
High–state voltage drop	$V_{CC} = V_{CC(\text{min})} + 0.2\text{ V}$ , $R_{\text{DRV}} = 33\text{ k}\Omega$ , DRV high	$V_{\text{DRV}(\text{drop})}$	–	–	1	V

## CURRENT SENSE

Input Pull–up Current	$V_{CS} = 0.7\text{ V}$	$I_{\text{bias}}$	–	1	–	$\mu\text{A}$
Maximum internal current setpoint	$V_{FB} > 3.5\text{ V}$	$V_{\text{ILIM}}$	0.66	0.70	0.74	V
Propagation delay from $V_{\text{Ilimit}}$ detection to DRV off	$V_{CS} = V_{\text{ILIM}}$	$t_{\text{delay}}$	–	80	110	ns
Leading Edge Blanking Duration for $V_{\text{ILIM}}$		$t_{\text{LEB}}$	200	250	320	ns
Threshold for immediate fault protection activation		$V_{CS(\text{stop})}$	0.95	1.05	1.15	V
Leading Edge Blanking Duration for $V_{CS(\text{stop})}$ (Note 6)		$t_{\text{BCS}}$	90	120	150	ns
Soft–start duration	From 1 <sup>st</sup> pulse to $V_{CS} = V_{\text{ILIM}}$	$t_{\text{SSTART}}$	2.8	4	5.2	ms
Frozen current setpoint		$V_{\text{I}(\text{freeze})}$	275	300	325	mV

## INTERNAL SLOPE COMPENSATION

Slope of the compensation ramp		$S_{\text{comp}(65\text{kHz})}$	–	–32.5	–	$\text{mV} / \mu\text{s}$
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## FEEDBACK

Internal pull–up resistor	$T_J = 25^\circ\text{C}$	$R_{\text{FB}(\text{up})}$	15	20	25	$\text{k}\Omega$
$V_{FB}$ to internal current setpoint division ratio		$K_{\text{FB}}$	4.7	5	5.3	–
Internal pull–up voltage on the FB pin (Note 6)		$V_{\text{FB}(\text{ref})}$	4.5	5	5.5	V
Feedback voltage below which the peak current is frozen		$V_{\text{FB}(\text{freeze})}$	1.35	1.5	1.65	V

## SKIP CYCLE MODE

Feedback voltage thresholds for skip mode	$V_{\text{FB}}$ going down $V_{\text{FB}}$ going up	$V_{\text{skip}(\text{in})}$ $V_{\text{skip}(\text{out})}$	0.63 0.72	0.70 0.80	0.77 0.88	V
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## REMOTE CONTROL ON FB PIN

The voltage above which the part enters the on mode	$V_{CC} > V_{CC(\text{off})}$ , $V_{HV} = 60\text{ V}$	$V_{\text{ON}}$	–	2.2	–	V
The voltage below which the part enters the off mode	$V_{CC} > V_{CC(\text{off})}$	$V_{\text{OFF}}$	0.35	0.40	0.45	V
Minimum hysteresis between the $V_{\text{ON}}$ and $V_{\text{OFF}}$	$V_{CC} > V_{CC(\text{off})}$ , $V_{HV} = 60\text{ V}$	$V_{\text{HYST}}$	500	–	–	mV

- Internal supply current only, currents sourced via FB pin is not included (current is flowing in GND pin only).
- Guaranteed by design.
- CS pin source current is a sum of  $I_{\text{bias}}$  and  $I_{\text{OPC}}$ , thus at  $V_{HV} = 125\text{ V}$  is observed the  $I_{\text{bias}}$  only, because  $I_{\text{OPC}}$  is switched off.

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**ELECTRICAL CHARACTERISTICS** (For typical values  $T_J = 25^\circ\text{C}$ , for min/max values  $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ ,  $V_{HV} = 125\text{ V}$ ,  $V_{CC} = 11\text{ V}$  unless otherwise noted)

Characteristics	Test Condition	Symbol	Min	Typ	Max	Unit
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### REMOTE CONTROL ON FB PIN

Pull-up current in off mode	$V_{CC} > V_{CC(\text{off})}$	$I_{\text{OFF}}$	–	5	–	$\mu\text{A}$
Go To Off mode timer	$V_{CC} > V_{CC(\text{off})}$	$t_{\text{GTOM}}$	500	600	800	ms

### OVERLOAD PROTECTION

Fault timer duration		$t_{\text{fault}}$	108	128	178	ms
Autorecovery mode latch-off time duration		$t_{\text{autorec}}$	0.85	1.00	1.35	s

### OVERPOWER PROTECTION

$V_{HV}$ to $I_{\text{OPC}}$ conversion ratio		$K_{\text{OPC}}$	–	0.54	–	$\mu\text{A} / \text{V}$
Current flowing out of CS pin (Note 7)	$V_{HV} = 125\text{ V}$	$I_{\text{OPC}(125)}$	–	0	–	$\mu\text{A}$
	$V_{HV} = 162\text{ V}$	$I_{\text{OPC}(162)}$	–	20	–	
	$V_{HV} = 325\text{ V}$	$I_{\text{OPC}(325)}$	–	110	–	
	$V_{HV} = 365\text{ V}$	$I_{\text{OPC}(365)}$	105	130	150	
FB voltage above which $I_{\text{OPC}}$ is applied	$V_{HV} = 365\text{ V}$	$V_{\text{FB}(\text{OPCF})}$	2.12	2.35	2.58	V
FB voltage below which is no $I_{\text{OPC}}$ applied	$V_{HV} = 365\text{ V}$	$V_{\text{FB}(\text{OPCE})}$	–	2.15	–	V

### LATCH-OFF INPUT

High threshold	$V_{\text{Latch}}$ going up	$V_{\text{OVP}}$	2.35	2.5	2.65	V
Low threshold	$V_{\text{Latch}}$ going down	$V_{\text{OTP}}$	0.76	0.8	0.84	V
Current source for direct NTC connection During normal operation During soft-start	$V_{\text{Latch}} = 0\text{ V}$	$I_{\text{NTC}}$	65	95	105	$\mu\text{A}$
		$I_{\text{NTC}(\text{SSTART})}$	130	190	210	
Blanking duration on high latch detection		$t_{\text{Latch}(\text{OVP})}$	35	50	70	$\mu\text{s}$
Blanking duration on low latch detection		$t_{\text{Latch}(\text{OTP})}$	–	350	–	$\mu\text{s}$
Clamping voltage	$I_{\text{Latch}} = 0\text{ mA}$ $I_{\text{Latch}} = 1\text{ mA}$	$V_{\text{clamp}0(\text{Latch})}$	1.0	1.2	1.4	V
		$V_{\text{clamp}1(\text{Latch})}$	1.8	2.4	3.0	

### TEMPERATURE SHUTDOWN

Temperature shutdown	$T_J$ going up	$T_{\text{TSD}}$	–	150	–	$^\circ\text{C}$
Temperature shutdown hysteresis	$T_J$ going down	$T_{\text{TSD}(\text{HYS})}$	–	30	–	$^\circ\text{C}$

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7. CS pin source current is a sum of  $I_{\text{bias}}$  and  $I_{\text{OPC}}$ , thus at  $V_{HV} = 125\text{ V}$  is observed the  $I_{\text{bias}}$  only, because  $I_{\text{OPC}}$  is switched off.

TYPICAL CHARACTERISTIC



Figure 3. Minimum Current Source Operation  
 $V_{HV(min)}$



Figure 4. Off-State Leakage Current  $I_{start(off)}$

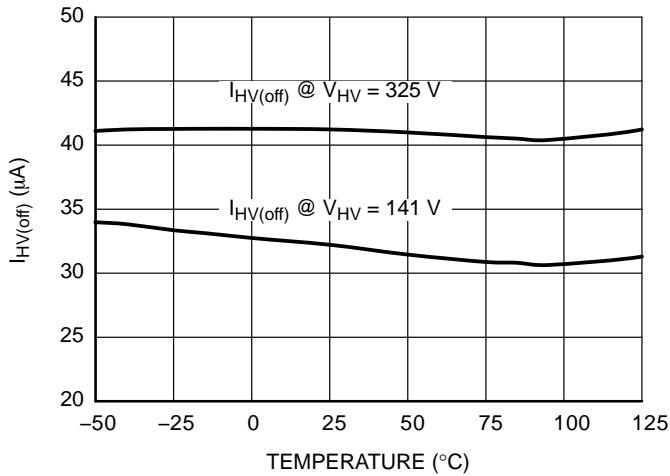


Figure 5. Off-Mode HV Supply Current  $I_{HV(off)}$

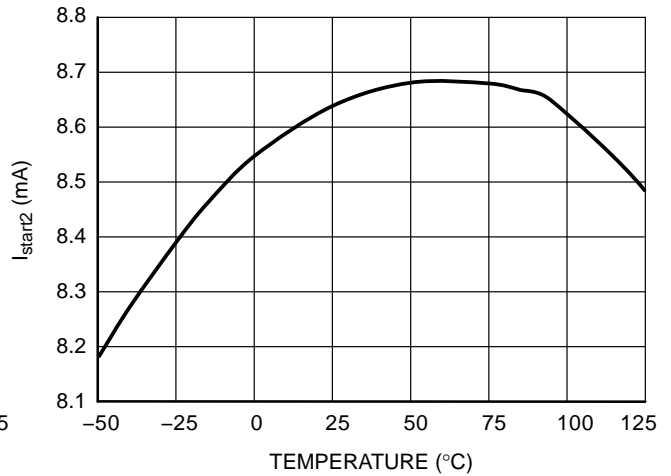


Figure 6. High Voltage Startup Current Flowing Out of  $V_{CC}$  Pin  $I_{start2}$

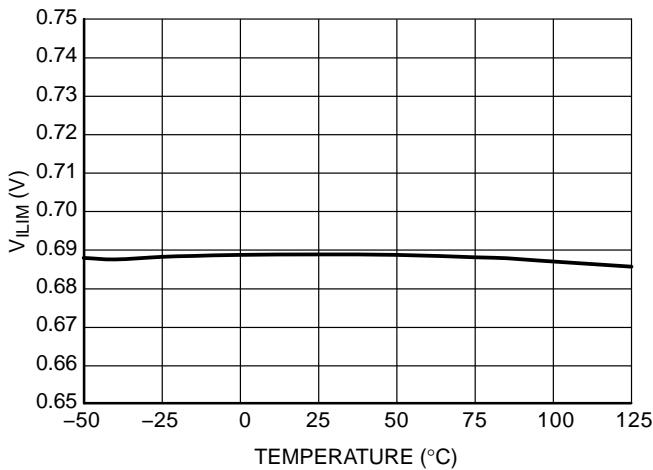


Figure 7. Maximum Internal Current Setpoint  
 $V_{ILIM}$

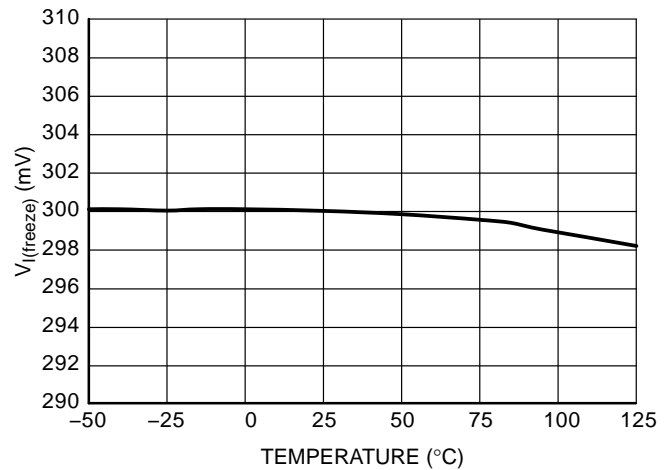


Figure 8. Frozen Current Setpoint  $V_{I(freeze)}$  for the Light Load Operation



TYPICAL CHARACTERISTIC

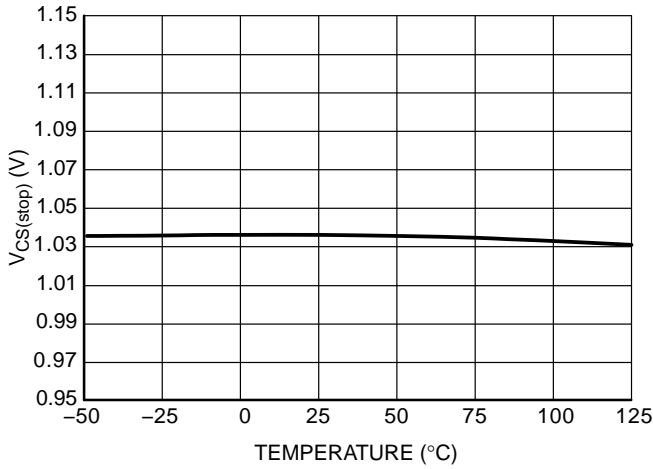


Figure 9. Threshold for Immediate Fault Protection Activation  $V_{CS(stop)}$

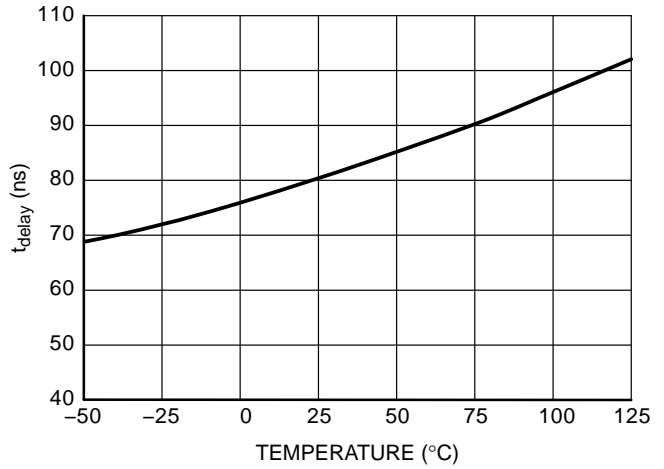


Figure 10. Propagation Delay  $t_{delay}$

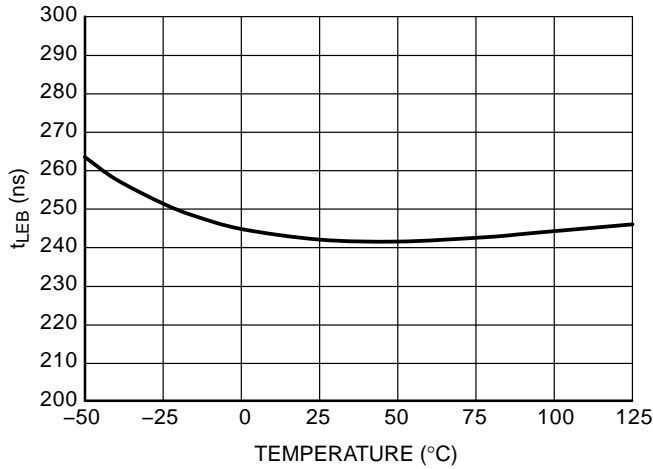


Figure 11. Leading Edge Blanking Duration  $t_{LEB}$

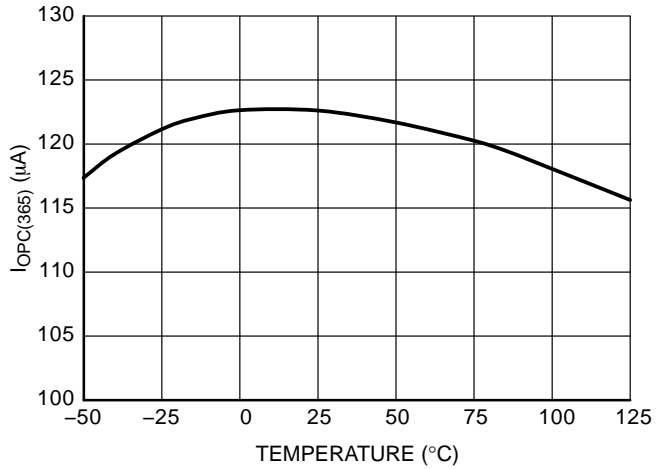


Figure 12. Maximum Overpower Compensating Current  $I_{OP(365)}$  Flowing Out of CS Pin

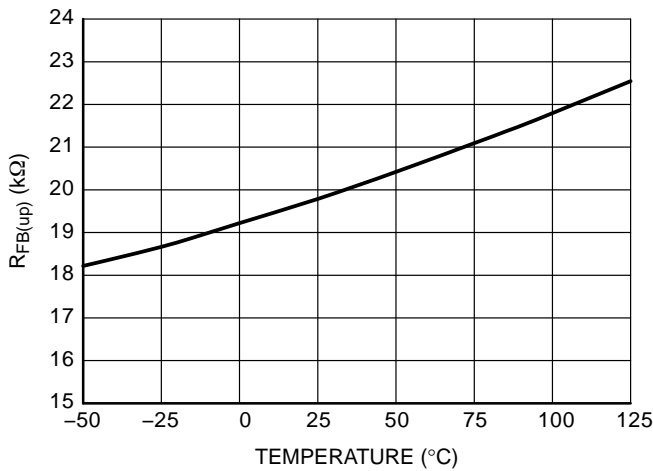


Figure 13. FB Pin Internal Pull-up Resistor  $R_{FB(up)}$

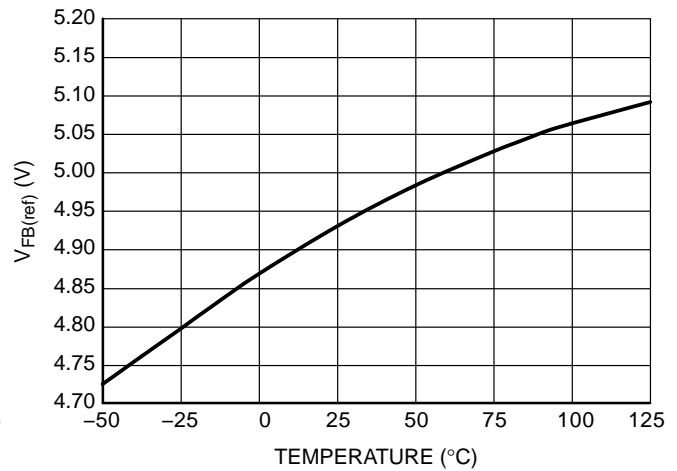


Figure 14. FB Pin Open Voltage  $V_{FB(ref)}$

TYPICAL CHARACTERISTIC

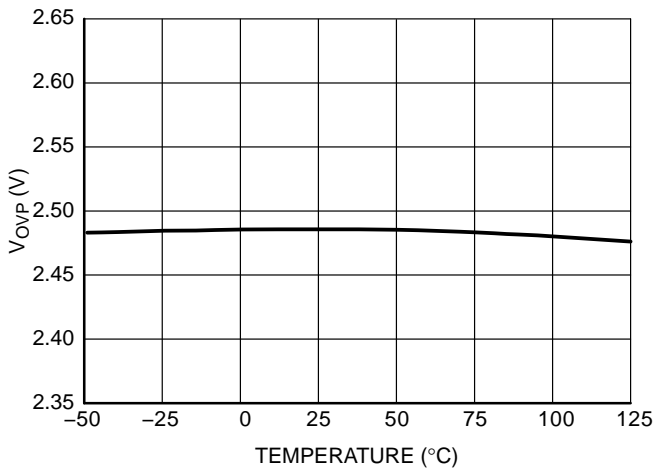


Figure 15. Latch Pin High Threshold  $V_{OVP}$

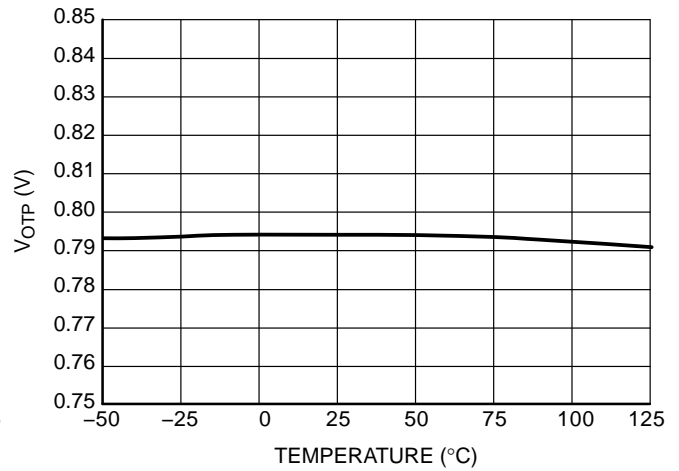


Figure 16. Latch Pin Low Threshold  $V_{OTP}$

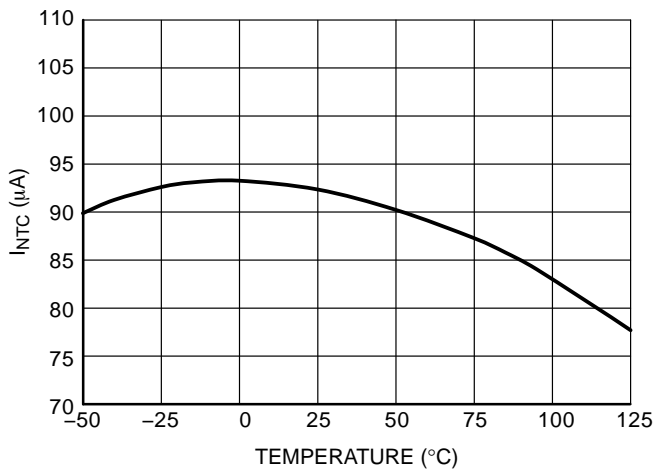


Figure 17. Current  $I_{NTC}$  Sourced from the Latch Pin, Allowing Direct NTC Connection

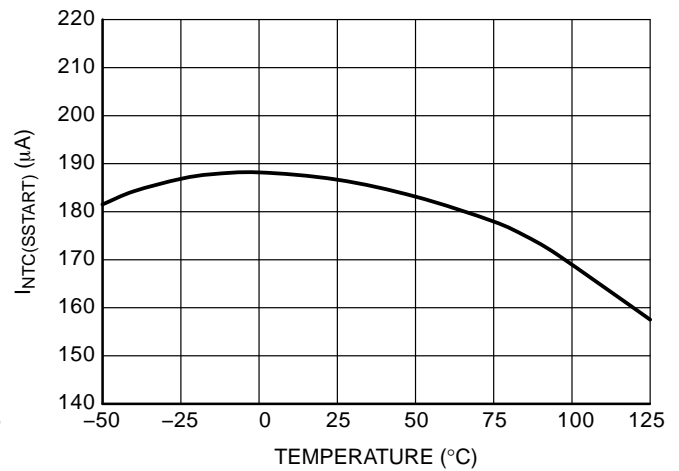


Figure 18. Current  $I_{NTC(SSSTART)}$  Sourced from the Latch Pin, During Soft-Start

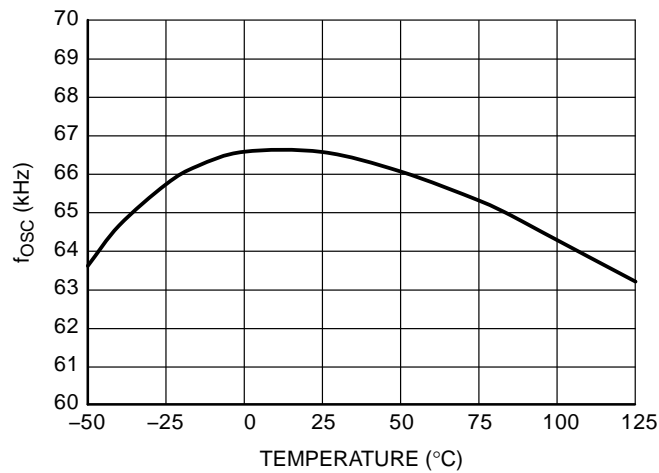


Figure 19. Oscillator Frequency  $f_{osc}$

TYPICAL CHARACTERISTIC

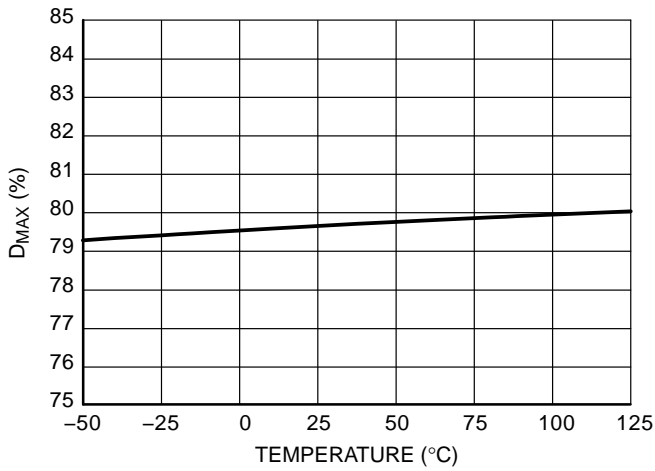


Figure 20. Maximum Duty Ratio  $D_{MAX}$

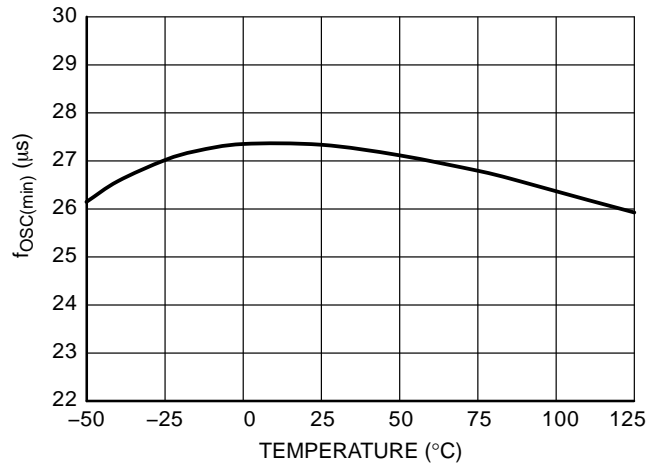


Figure 21. Minimum Switching Frequency  $f_{osc(min)}$

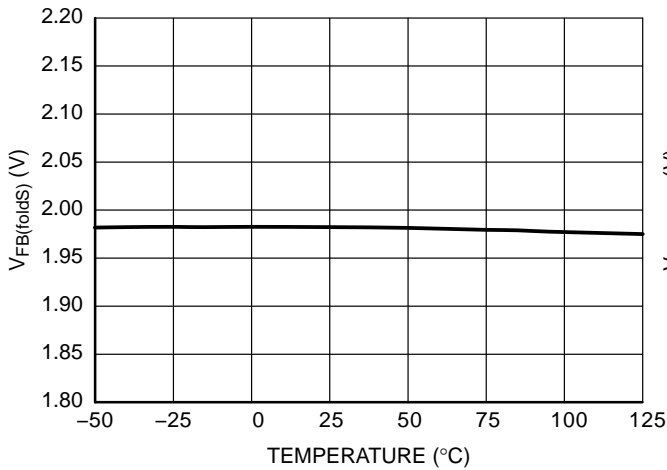


Figure 22. FB Pin Voltage Below Which Frequency Foldback Starts  $V_{FB(foldS)}$

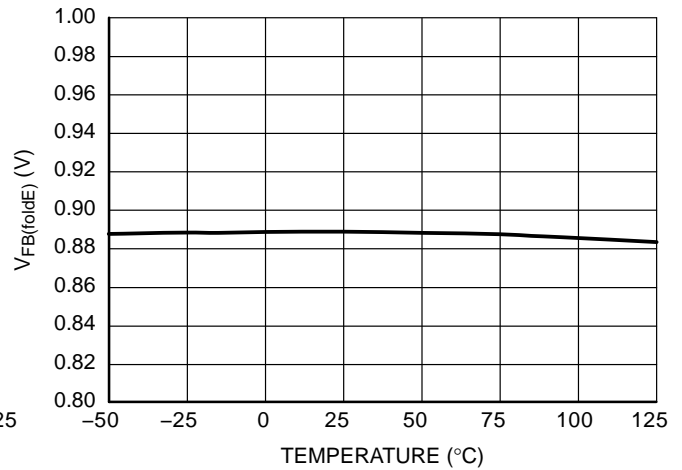


Figure 23. FB Pin Voltage Below Which Frequency Foldback Complete  $V_{FB(foldE)}$

TYPICAL CHARACTERISTIC

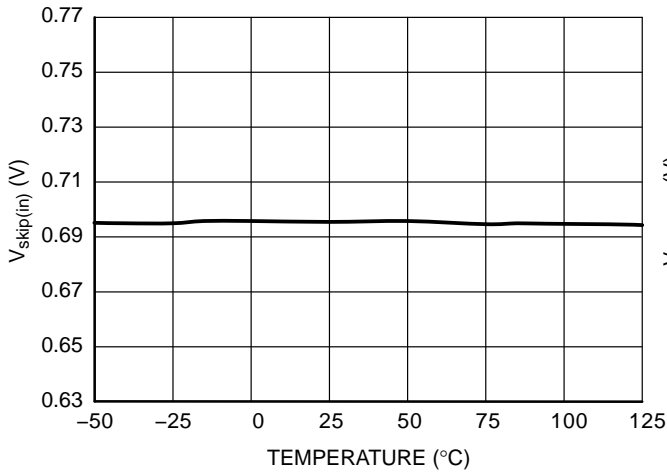


Figure 24. FB Pin Skip-In Level  $V_{skip(in)}$

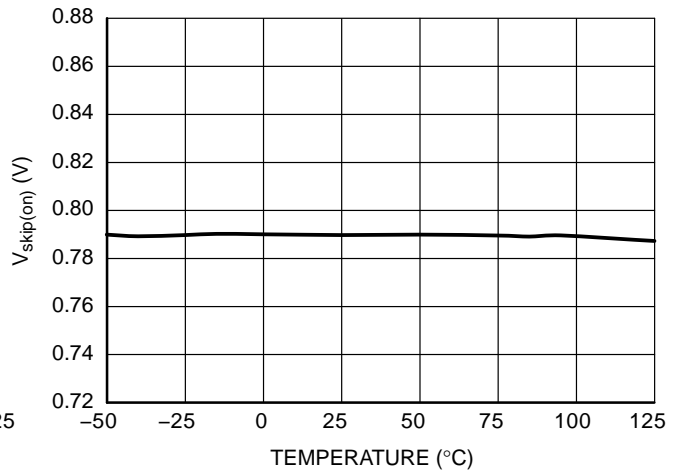


Figure 25. FB Pin Skip-Out Level  $V_{skip(out)}$

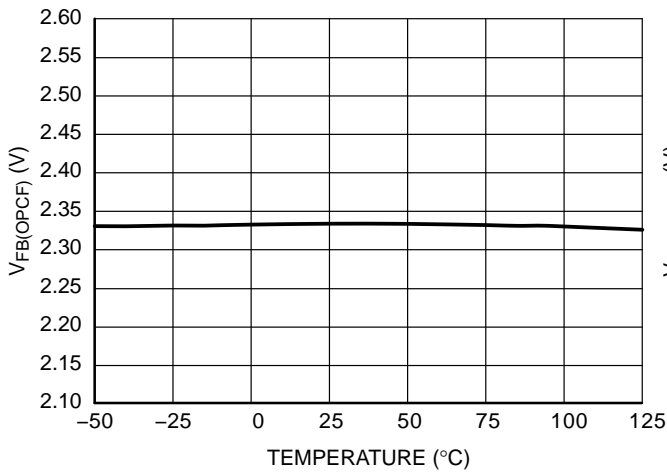


Figure 26. FB Pin Level  $V_{FB(OPCF)}$  Above Which is the Overpower Compensation Applied

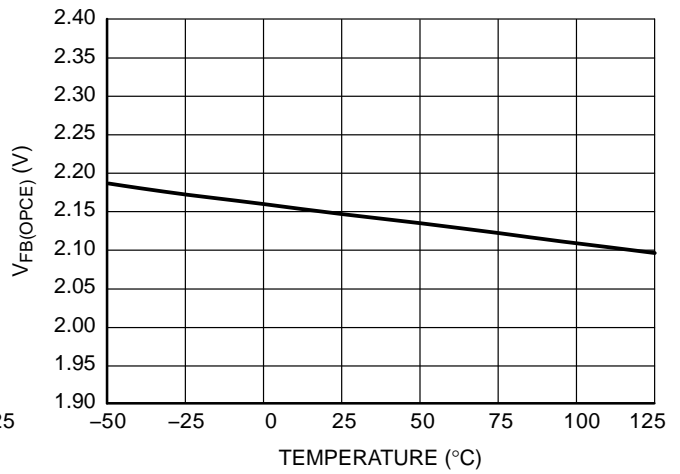


Figure 27. FB Pin Level  $V_{FB(OPCE)}$  Below Which is No Overpower Compensation Applied

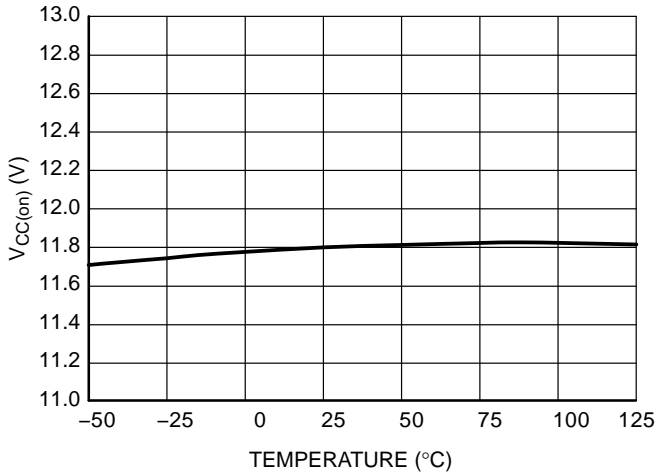


Figure 28.  $V_{CC}$  Turn-on Threshold Level,  $V_{CC}$  Going Up HV Current Source Stop Threshold  $V_{CC(on)}$

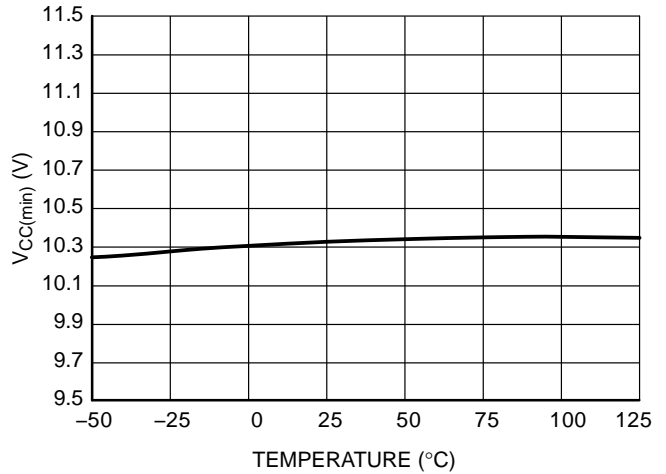


Figure 29. HV Current Source Restart Threshold  $V_{CC(min)}$

TYPICAL CHARACTERISTIC

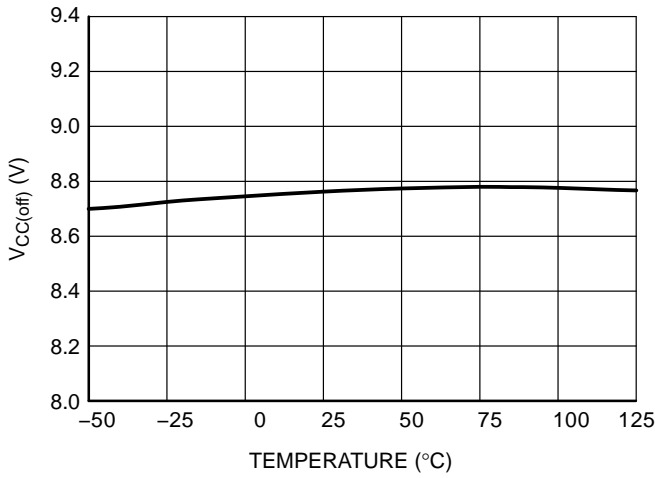


Figure 30.  $V_{CC}$  Turn-off Threshold (UVLO)  
 $V_{CC(off)}$

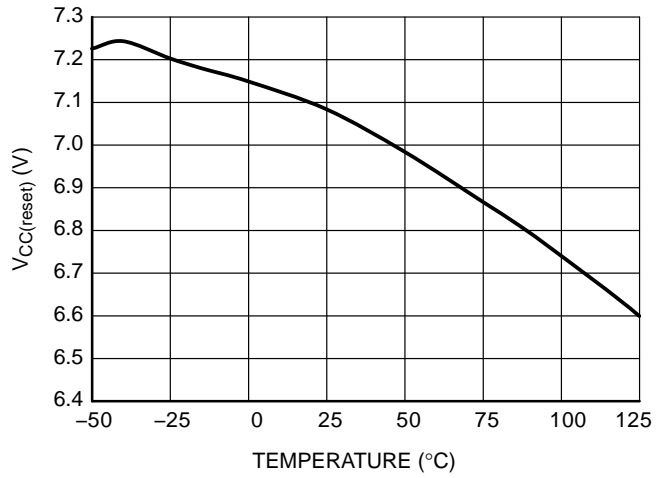


Figure 31.  $V_{CC}$  Decreasing Level at Which the Internal Logic Resets  $V_{CC(reset)}$

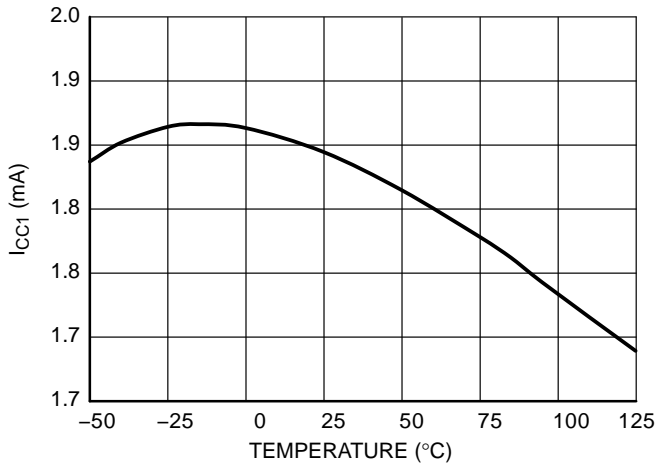


Figure 32. Internal Current Consumption when DRV Pin is Unloaded

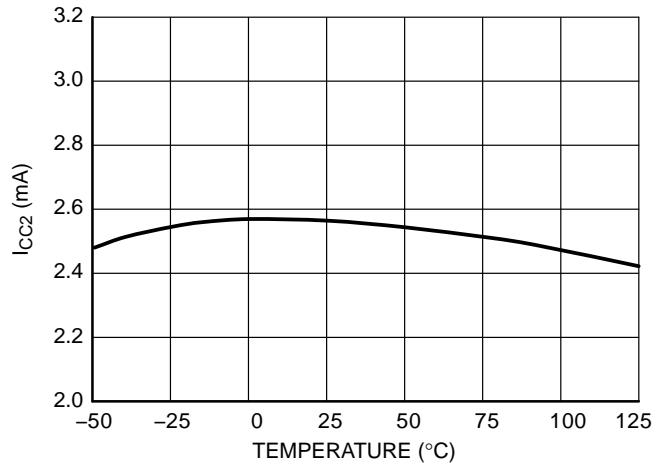


Figure 33. Internal Current Consumption when DRV Pin is Loaded by 1 nF

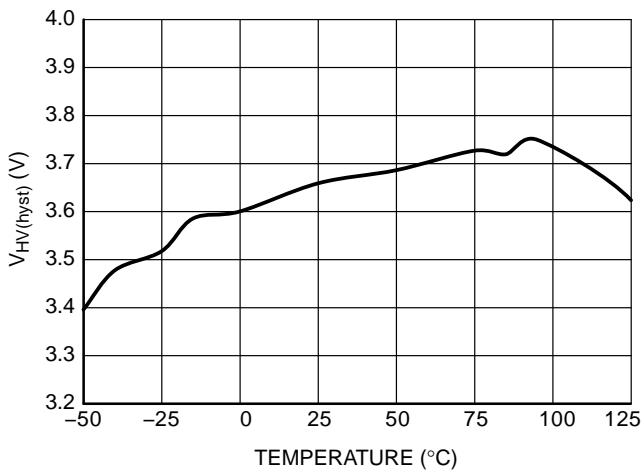


Figure 34. X2 Discharge Comparator Hysteresis Observed at HV Pin  $V_{HV(hyst)}$

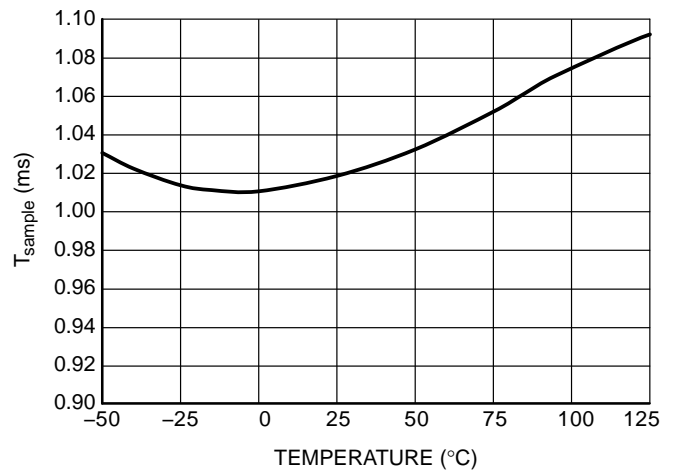


Figure 35. HV Signal Sampling Period  $T_{sample}$

TYPICAL CHARACTERISTIC

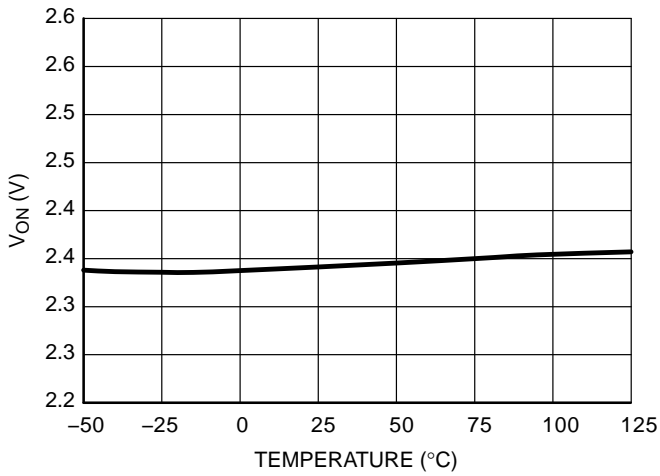


Figure 36. FB Pin Voltage Level Above Which is Entered On Mode  $V_{ON}$

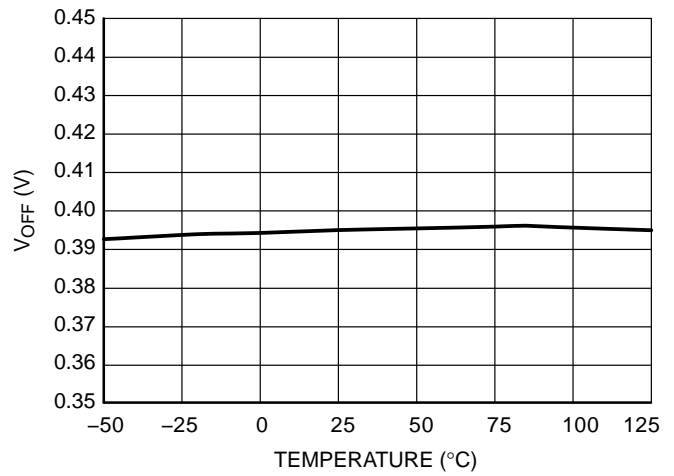


Figure 37. FB Pin Voltage Level Below Which is Entered Off Mode  $V_{OFF}$

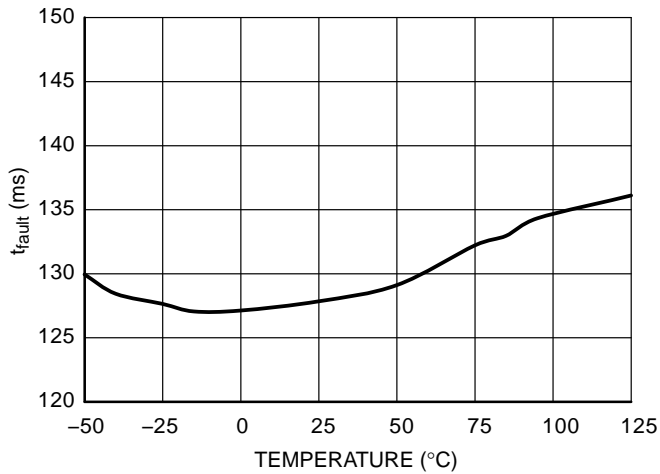


Figure 38. Fault Timer Duration  $t_{fault}$

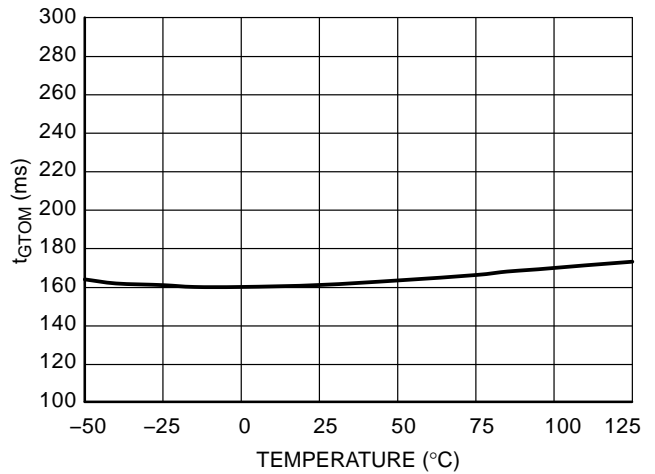


Figure 39. Go To Off Mode Timer Duration  $t_{GTOM}$

APPLICATION INFORMATION

Functional Description

The SCY99194 includes all necessary features to build a safe and efficient power supply based on a fixed-frequency flyback converter. The SCY99194 is a multimode controller as illustrated in Figure 40. The mode of operation depends upon line and load condition. Under all modes of operation, the SCY99194 terminates the DRV signal based on the switch current. Thus, the SCY99194 always operates in current mode control so that the power MOSFET current is always limited.

Under normal operating conditions, the FB pin commands the operating mode of the SCY99194 at the voltage thresholds shown in Figure 40. At normal rated operating loads (from 100% to approximately 33% full rated power) the SCY99194 controls the converter in fixed frequency PWM mode. It can operate in the continuous conduction mode (CCM) or discontinuous conduction mode (DCM) depending upon the input voltage and loading conditions. If the controller is used in CCM with a wide input voltage range, the duty-ratio may increase up to 50%. The build-in slope compensation prevents the appearance of sub-harmonic oscillations in this operating area.

For loads that are between approximately 32% and 10% of full rated power, the converter operates in frequency foldback mode (FFM). If the feedback pin voltage is lower than 1.5 V the peak switch current is kept constant and the output voltage is regulated by modulating the switching frequency for a given and fixed input voltage  $V_{HV}$ .

Effectively, operation in FFM results in the application of constant volt-seconds to the flyback transformer each switching cycle. Voltage regulation in FFM is achieved by varying the switching frequency in the range from 65 kHz to 27 kHz. For extremely light loads (below approximately 6% full rated power), the converter is controlled using bursts of 27 kHz pulses. This mode is called as skip mode. The FFM, keeping constant peak current and skip mode allows design of the power supplies with increased efficiency under the light loading conditions. Keep in mind that the aforementioned boundaries of steady-state operation are approximate because they are subject to converter design parameters.

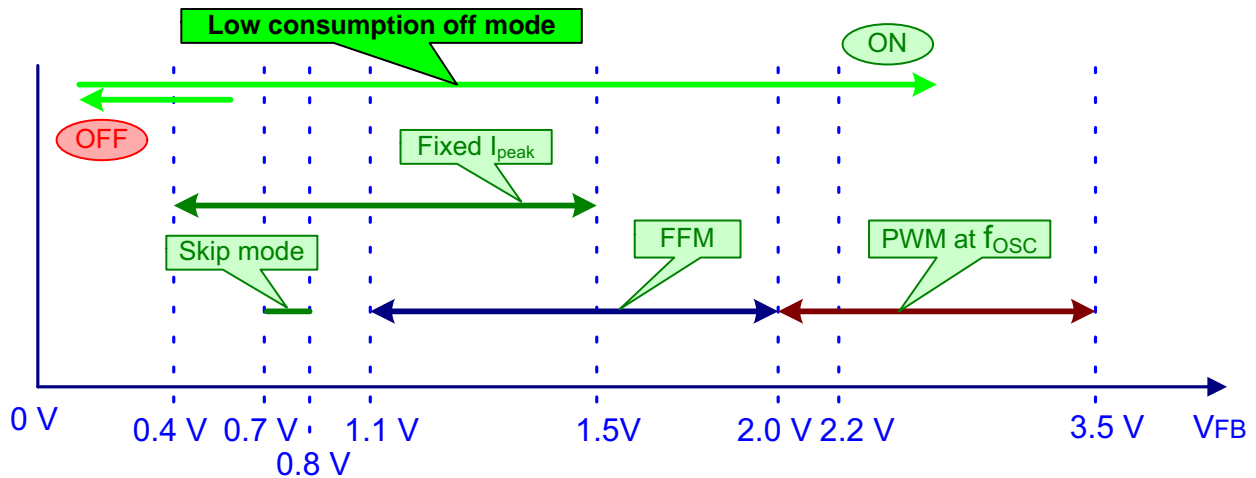


Figure 40. Mode Control with FB pin voltage

There was implemented the low consumption off mode allowing to reach extremely low no load input power. This mode is controlled by the FB pin and allows the remote control (or secondary side control) of the power supply shut-down. Most of the device internal circuitry is unbiased in the low consumption off mode. Only the FB pin control circuitry and X2 cap discharging circuitry is operating in the low consumption off mode. If the voltage at feedback pin

decreases below the 0.4 V the controller will enter the low consumption off mode. The controller can start if the FB pin voltage increases above the 2.2 V level.

See the detailed status diagrams for the both versions fully latched A and the autorecovery B on the following figures. The basic status of the device after wake-up by the  $V_{CC}$  is the off mode and mode is used for the overheating protection mode if the thermal shutdown protection is activated.

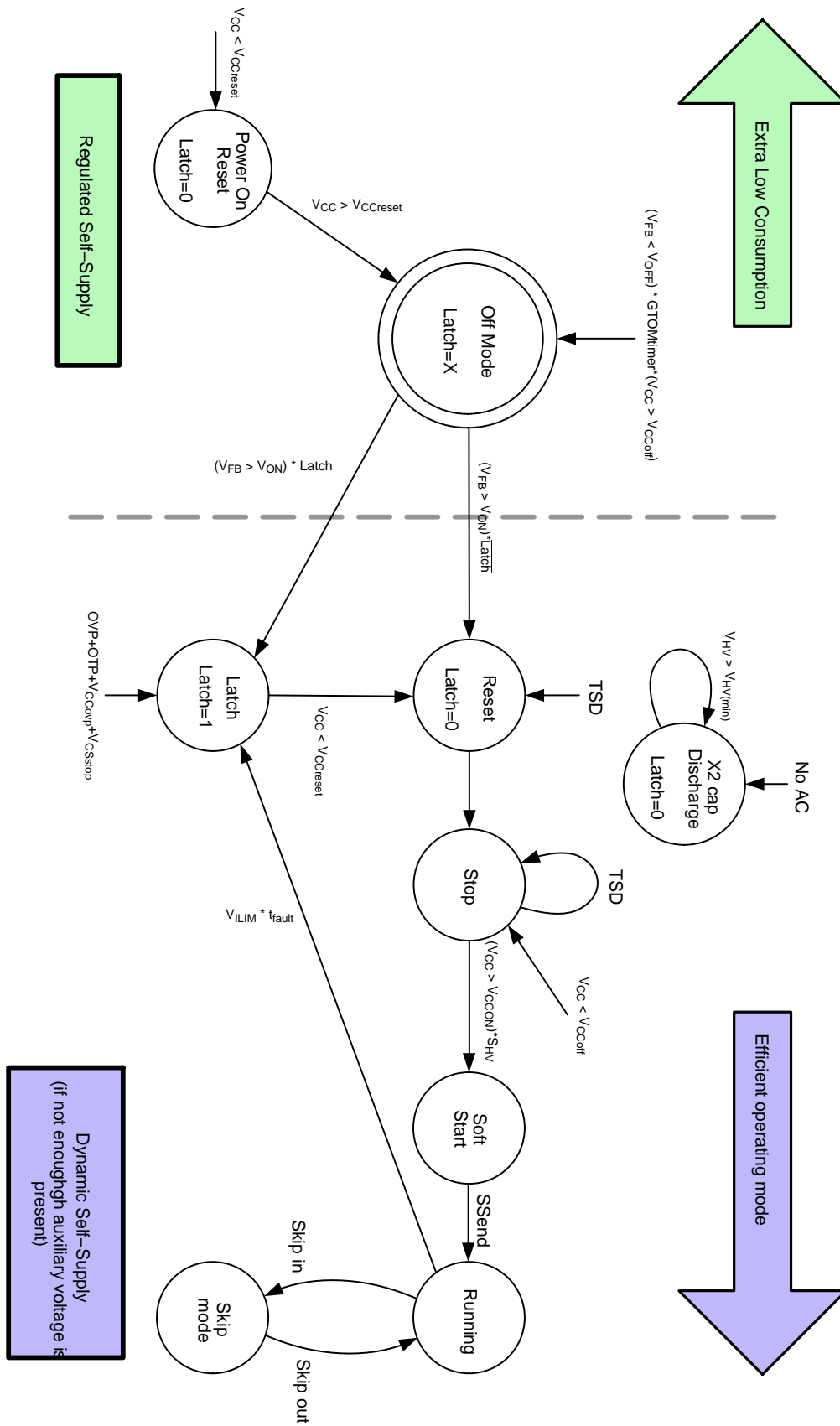


Figure 41. Operating Status Diagram for the Fully Latched Version A of the Device



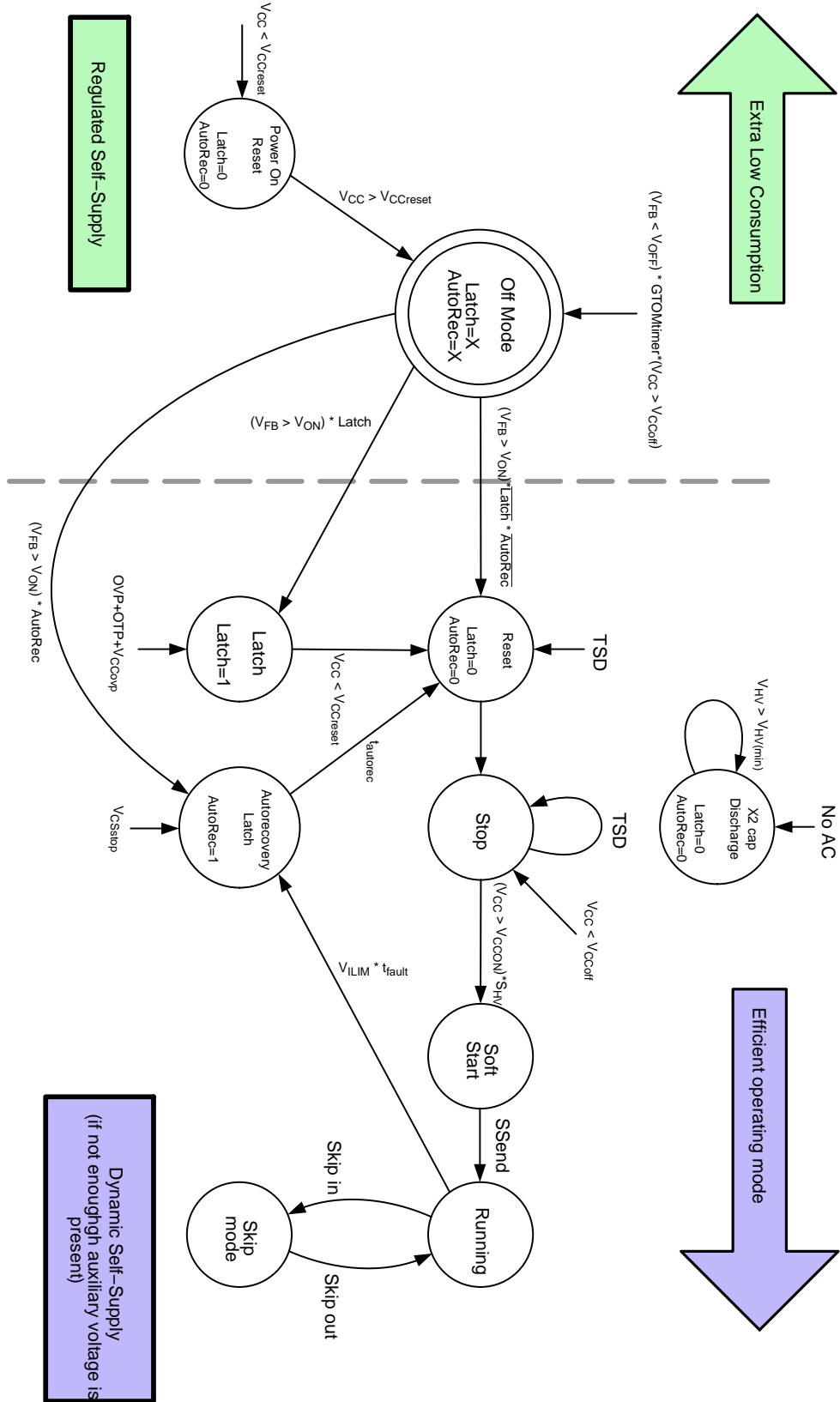


Figure 42. Operating Status Diagram for the Autorecovery Version B of the Device

The information about the fault (permanent Latch or Autorecovery) is kept during the low consumption off mode due the safety reason. The reason is not to allow unlatch the device by the remote control being in off mode.

**Start-up of the Controller**

At start-up, the current source turns on when the voltage on the HV pin is higher than  $V_{HV(min)}$ , and turns off when  $V_{CC}$  reaches  $V_{CC(on)}$ , then turns on again when  $V_{CC}$  reaches  $V_{CC(min)}$ , until  $V_{CC}$  is supplied by an external source. The controller actually starts the first time  $V_{CC}$  reaches  $V_{CC(on)}$  when the slope on HV pin is positive.

Even though the Dynamic Self-Supply is able to maintain the  $V_{CC}$  voltage between  $V_{CC(on)}$  and  $V_{CC(min)}$  by turning

the HV start-up current source on and off, it can only be used in light load condition, otherwise the power dissipation on the die would be too much. As a result, an auxiliary voltage source is needed to supply  $V_{CC}$  during normal operation.

The Dynamic Self-Supply is useful to keep the controller alive when no switching pulses are delivered, e.g. in latch or fault condition, or to prevent the controller from stopping during load transients when the  $V_{CC}$  might drop. The SCY99194 accepts a supply voltage as high as 28 V, with an overvoltage threshold  $V_{CC(ovp)}$  that latches the controller off.

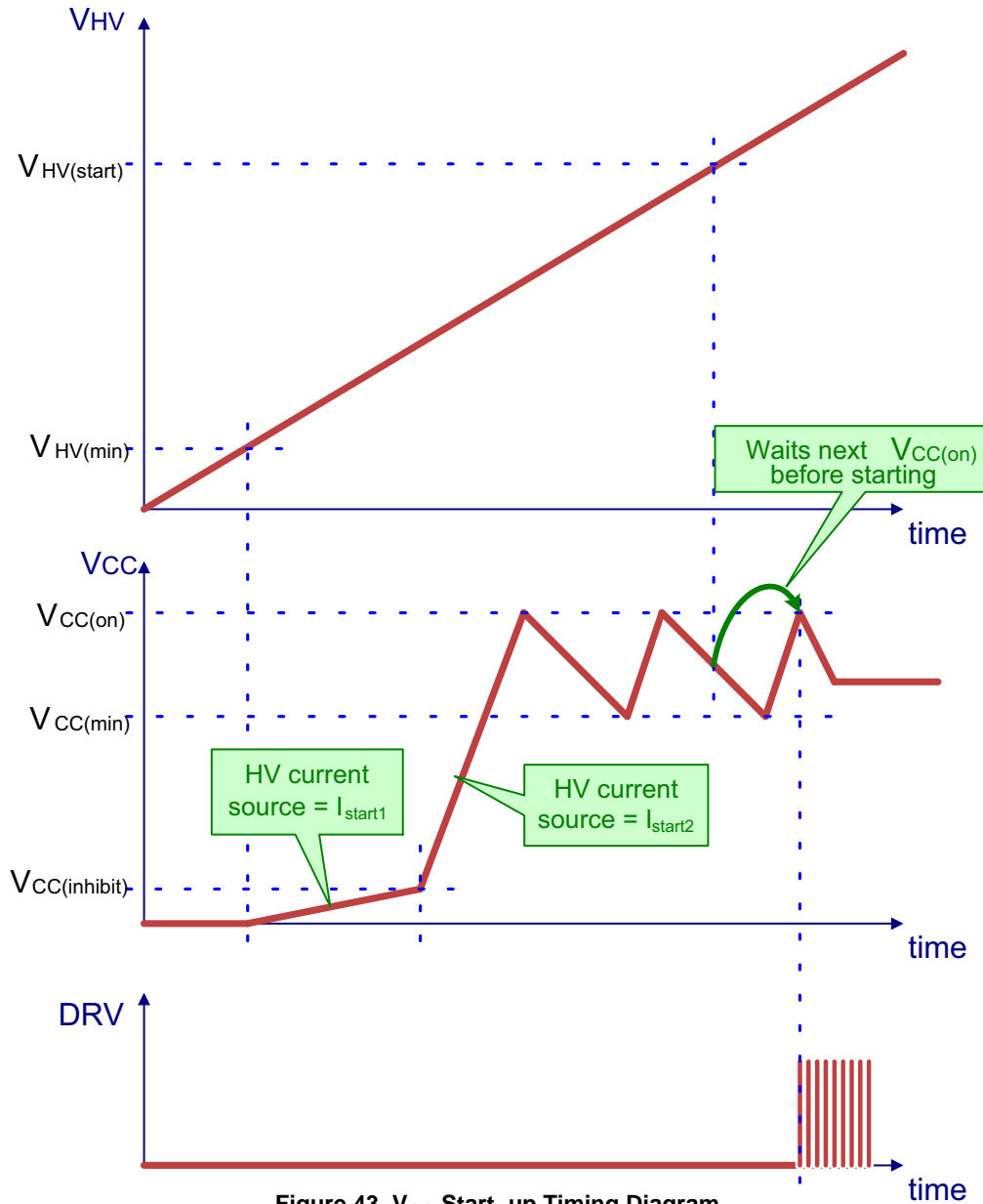


Figure 43.  $V_{CC}$  Start-up Timing Diagram

For safety reasons, the start-up current is lowered when  $V_{CC}$  is below  $V_{CC(inhibit)}$ , to reduce the power dissipation in case the  $V_{CC}$  pin is shorted to GND (in case of  $V_{CC}$  capacitor failure, or external pull-down on  $V_{CC}$  to disable the controller). There is only one condition for which the current source doesn't turn on when  $V_{CC}$  reaches  $V_{CC(inhibit)}$ : the voltage on HV pin is too low (below  $V_{HV(min)}$ ). The controller can restart only when  $V_{CC}$  reaches  $V_{CC(on)}$  and

when the slope on HV pin is positive during the short ac line drop-outs. This feature differentiates between the short ac line drop-outs and application plug off. The minimum positive slope is defined by the Equation 1 in following chapter.

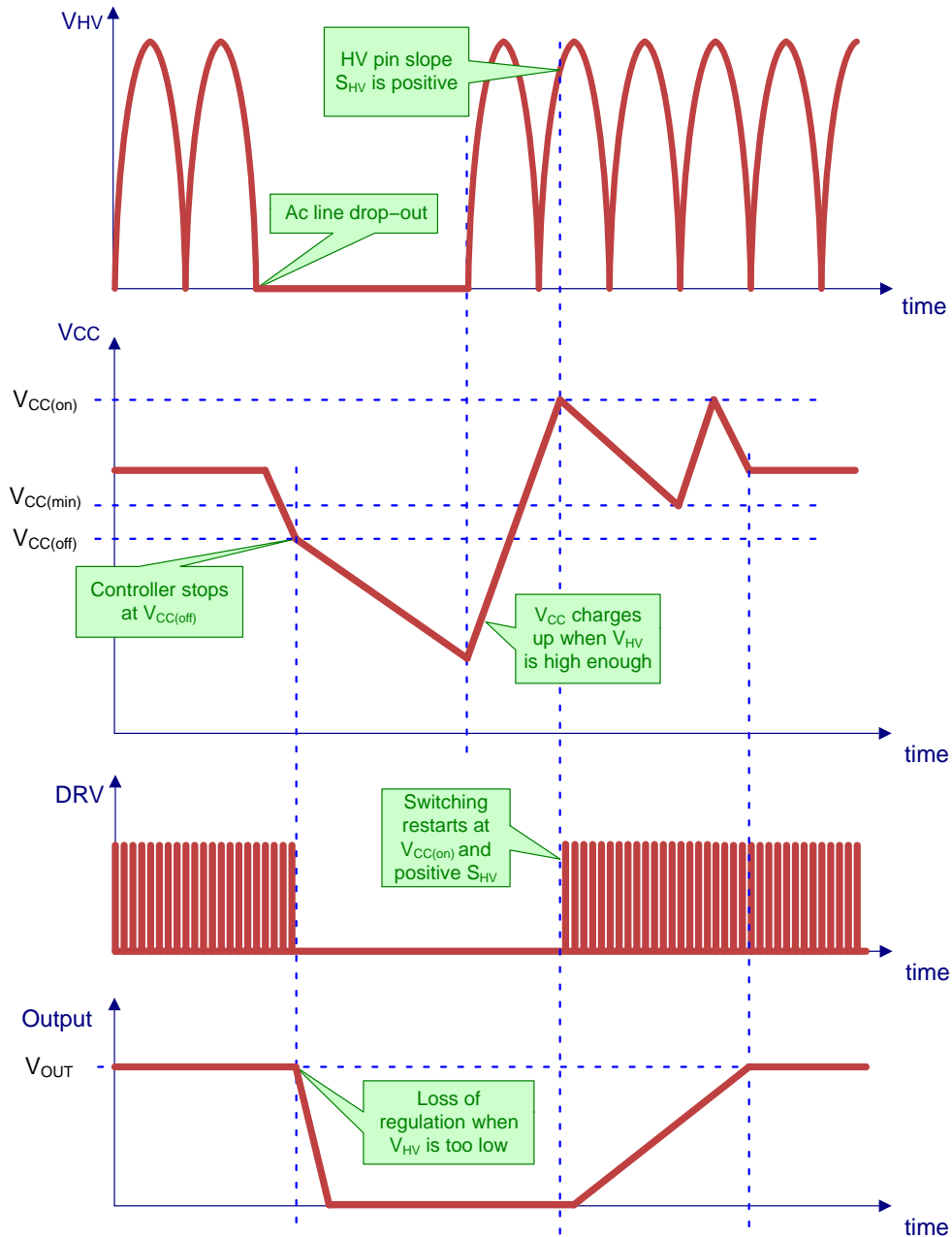


Figure 44. Ac Line Drop-out Timing Diagram

**X2 Cap Discharge Feature**

The X2 capacitor discharging feature is offered by usage of the SCY99194. This feature save approx. 16 mW – 25 mW input power depending on the EMI filter X2 capacitors volume and it saves the external components count as well. The discharge feature is ensured via the start-up current source with a dedicated control circuitry for this function.

There is used a dedicated structure called ac line unplug detector inside the X2 capacitor discharge control circuitry. See the Figure 45 for the block diagram for this structure and Figures 46, 47 and 49 for the timing diagrams. The basic idea of ac line unplug detector lies in comparison of the direct sample of the high voltage obtained via the high voltage sensing structure with the delayed sample of the high voltage. The delayed signal is created by the sample & hold structure.

The comparator used for the comparison of these signals is without hysteresis inside. The resolution between the slopes of the ac signal and dc signal is defined by the sampling time  $T_{SAMPLE}$  and additional internal offset  $N_{OS}$ . These parameters ensure the noise immunity as well. The additional offset is added to the picture of the sampled HV signal and its analog sum is stored in the  $C_1$  storage capacitor. If the voltage level of the HV sensing structure output crosses this level the comparator CMP output signal resets the detection timer and no dc signal is detected. The additional offset  $N_{OS}$  can be measured as the  $V_{HV(hyst)}$  on the HV pin. If the comparator output produces pulses it means that the slope of input signal is higher than set resolution level and the slope is positive. If the comparator output produces the low level it means that the slope of input signal is lower than set resolution level or the slope is negative. There is used the detection timer which is reset by any edge of the comparator output. It means if no edge comes before the timer elapses there is present only dc signal or signal with the small ac ripple at the HV pin. This type of the ac detector detects only the positive slope, which fulfils the requirements for the ac line presence detection.

In case of the dc signal presence on the high voltage input, there are the direct sample of the high voltage obtained via the high voltage sensing structure and the delayed sample of the high voltage equivalent and the comparator produces the low level signal during the presence of this signal. No edges are present at the output of the comparator, that's why the detection timer is not reset and dc detect signal appears.

The minimum detectable slope by this ac detector is given by the ration between the maximum hysteresis observed at HV pin  $V_{HV(hyst),max}$  and the sampling time:

$$S_{min} = \frac{V_{HV(hyst),max}}{T_{sample}} \quad (eq. 1)$$

Than it can be derived the relationship between the minimum detectable slope and the amplitude and frequency of the sinusoidal input voltage:

$$V_{max} = \frac{V_{HV(hyst),max}}{2 \cdot \pi \cdot f \cdot T_{sample}} = \frac{5}{2 \cdot \pi \cdot 35 \cdot 1 \cdot 10^{-3}} \quad (eq. 2)$$

$$= 22.7 \text{ V}$$

The minimum detectable AC RMS voltage is 16 V at frequency 35 Hz, if the maximum hysteresis is 5 V and sampling time is 1 ms.

The X2 capacitor discharge feature is available in any controller operation mode to ensure this safety feature. The detection timer is reused for the time limiting of the discharge phase, to protect the device against overheating. The discharging process is cyclic and continues until the ac line is detected again or the voltage across the X2 capacitor is lower than  $V_{HV(min)}$ . This feature ensures to discharge quite big X2 capacitors used in the input line filter to the safe level. **It is important to note that it is not allowed to connect HV pin to any dc voltage due this feature. e.g. directly to bulk capacitor.**

During the HV sensing or X2 cap discharging the  $V_{CC}$  net is kept above the  $V_{CC(off)}$  voltage by the Self-Supply in any mode of device operation to supply the control circuitry. During the discharge sequence device runs normally.

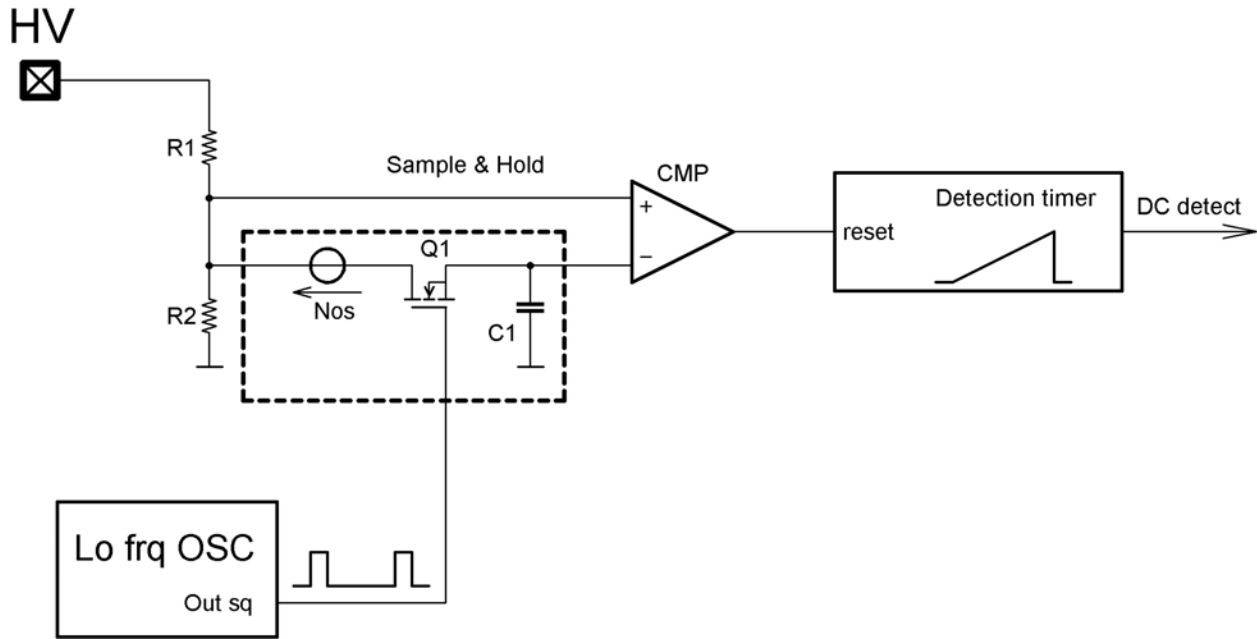


Figure 45. The ac Line Unplug Detector Structure Used for X2 Capacitor Discharge System

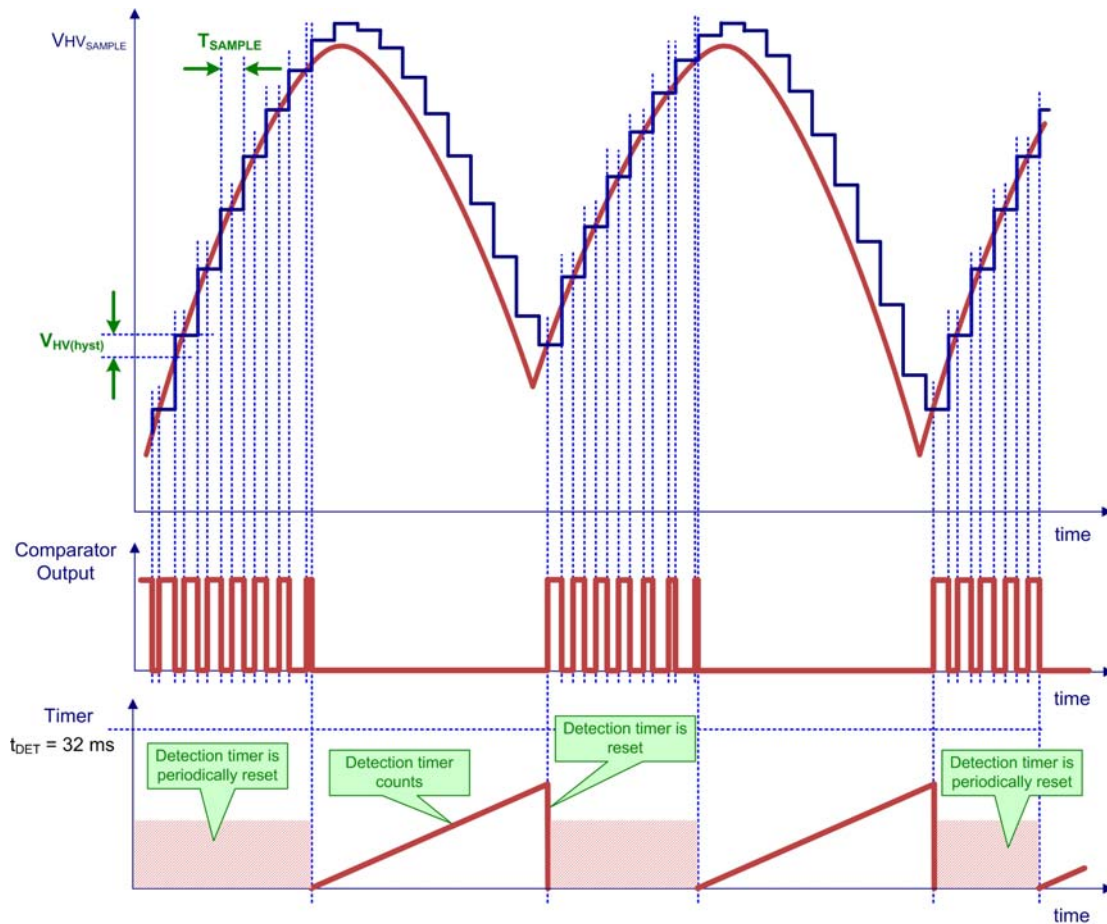


Figure 46. The ac Line Unplug Detector Timing Diagram



Figure 47. The ac Line Unplug Detector Timing Diagram Detail with Noise Effects

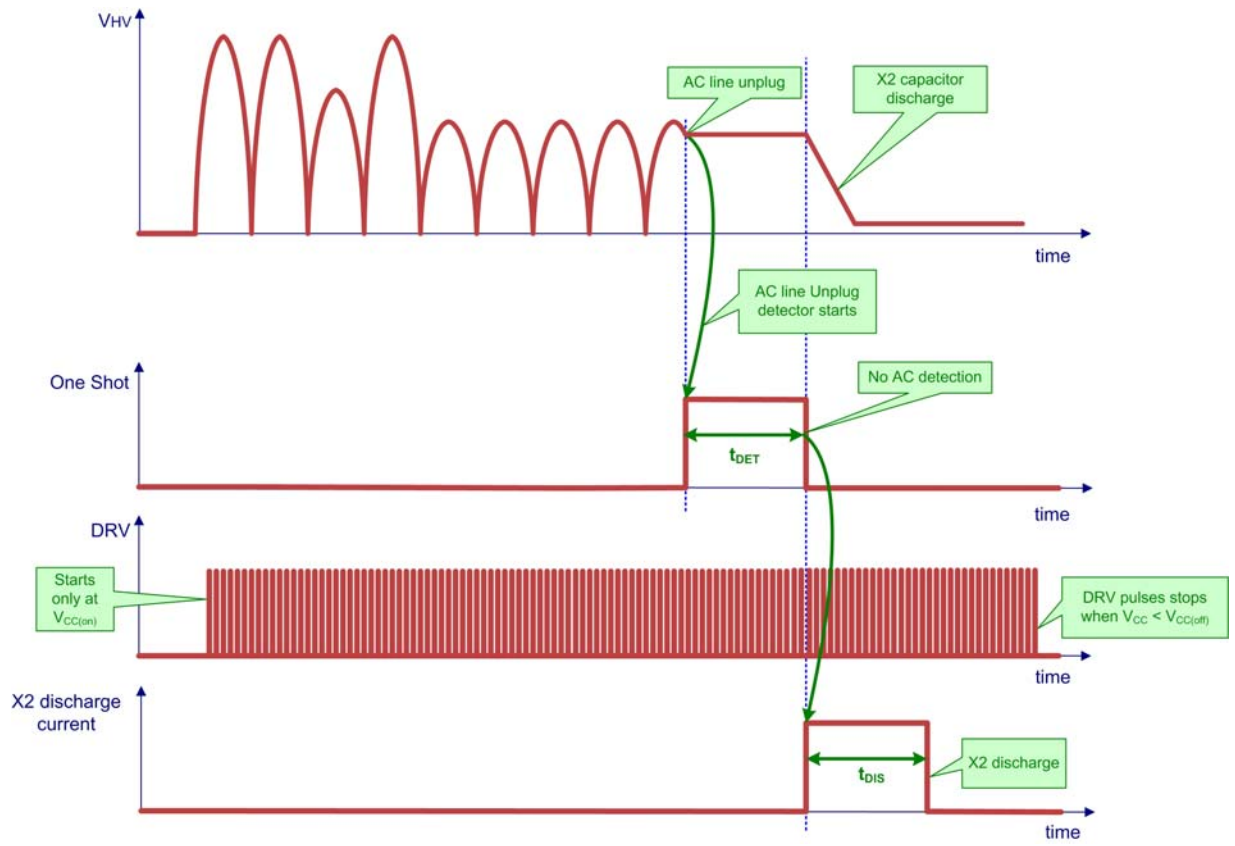


Figure 48. HV Pin ac Input Timing Diagram with X2 Capacitor Discharge Sequence when the Application is Unplugged Under Extremely Low Line Condition

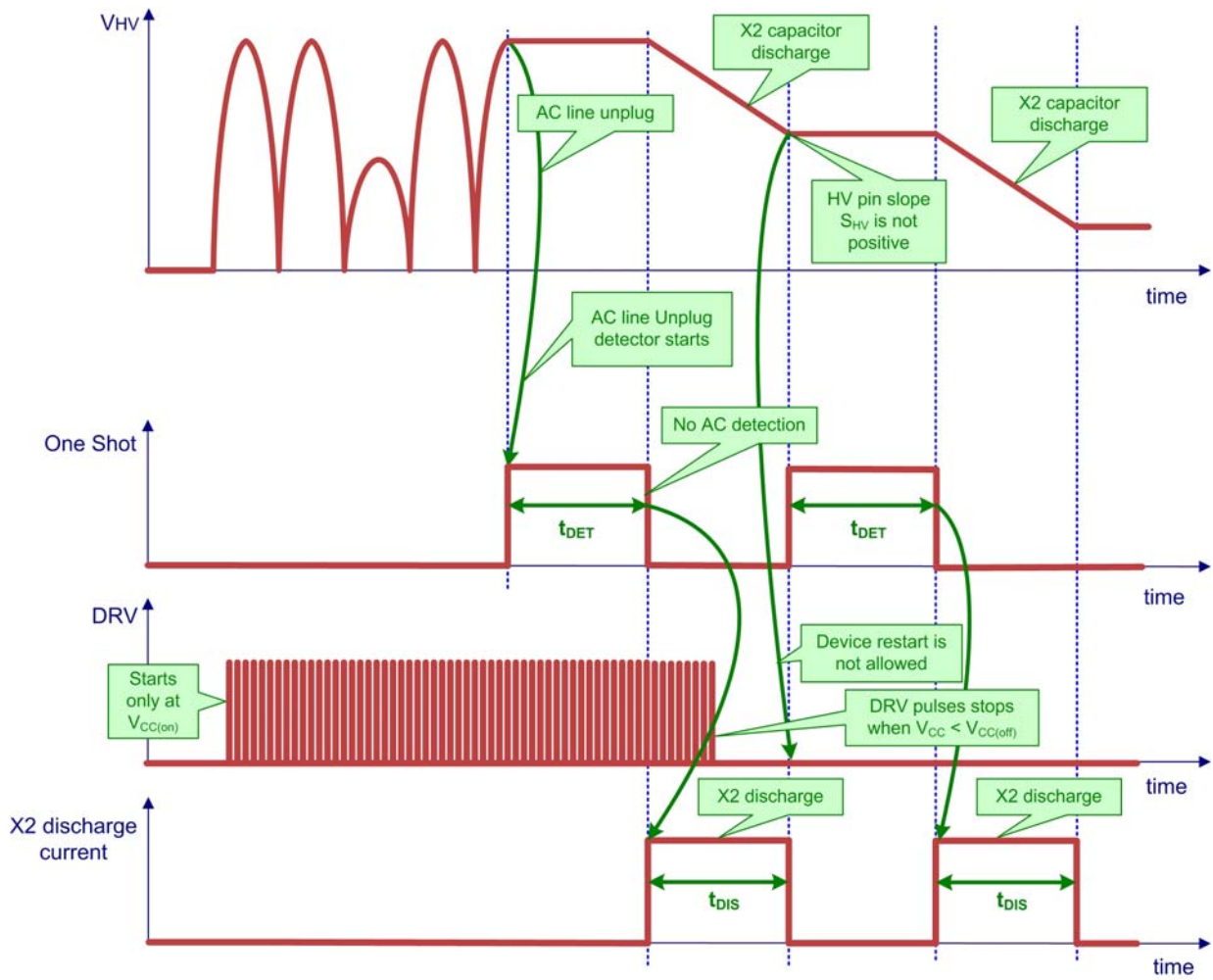
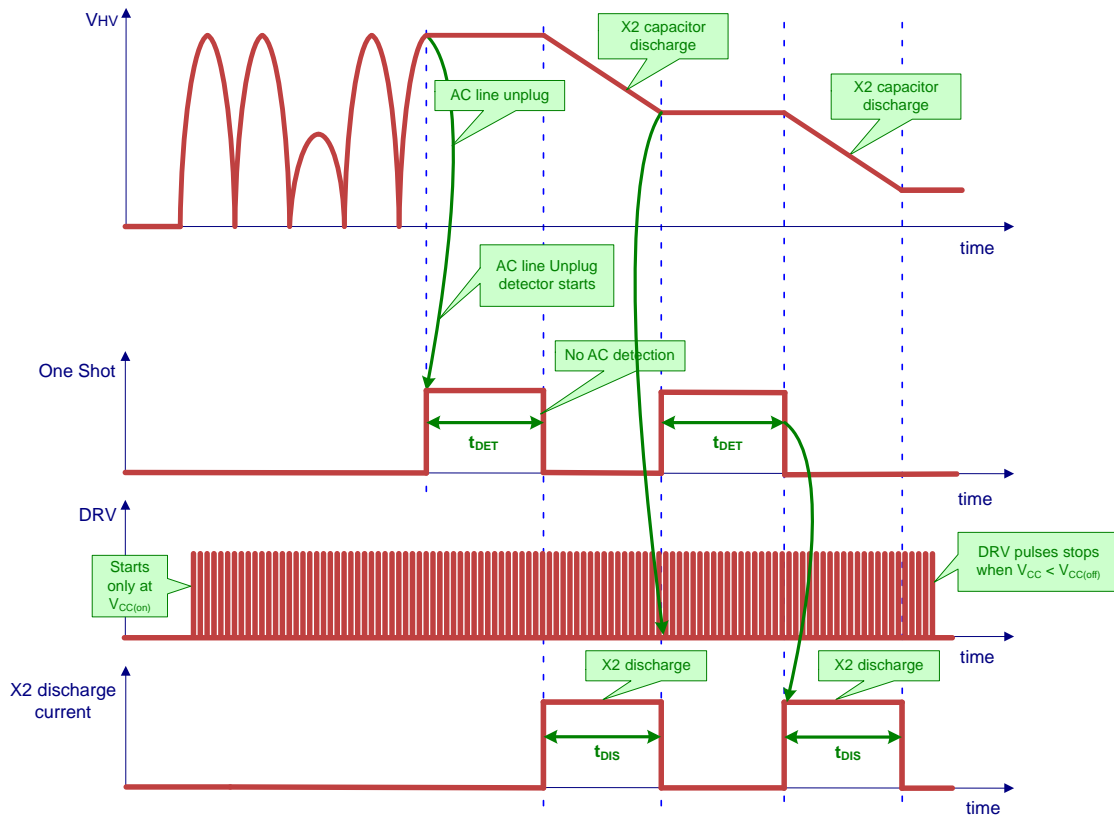


Figure 49. HV Pin ac Input Timing Diagram with X2 Capacitor Discharge Sequence When the Application is Unplugged Under High Line and Heavy Load Condition





**Figure 50. HV Pin ac Input Timing Diagram with X2 Capacitor Discharge Sequence When the Application is Unplugged Under High Line and Light Load Condition**

**The Low Consumption Off Mode**

There was implemented the low consumption off mode allowing to reach extremely low no load input power as described in previous chapters. If the voltage at feedback pin decreases below the 0.4 V the controller enters the off mode. The internal  $V_{CC}$  is turned-off, the IC consumes extremely low  $V_{CC}$  current and only the voltage at external  $V_{CC}$  capacitor is maintained by the Self-Supply circuit. The Self-Supply circuit keeps the  $V_{CC}$  voltage at the  $V_{CC(reg)}$  level. The supply for the FB pin watch dog circuitry and FB pin bias is provided via the low consumption current sources from the external  $V_{CC}$  capacitor. The controller can only start, if the FB pin voltage increases above the 2.2 V level. See Figure 51 for timing diagrams.

Only the X2 cap discharge and Self-Supply features is enabled in the low consumption off mode. The X2 cap

discharging feature is enable due the safety reasons and the DSS is enabled to keep the  $V_{CC}$  supply, but only very low  $V_{CC}$  consumption appears in this mode. See the  $I_{CC5}$  parameter in the electrical table. Any other features are disabled in this mode.

The information about the latch status of the device is kept in the low consumption off mode and this mode is used for the TSD protection as well. The protection timer GoToOffMode  $t_{GTOM}$  is used to protect the application against the false activation of the low consumption off mode by the fast drop outs of the FB pin voltage below the 0.4 V level. E.g. in case when is present high FB pin voltage ripple during the skip mode.

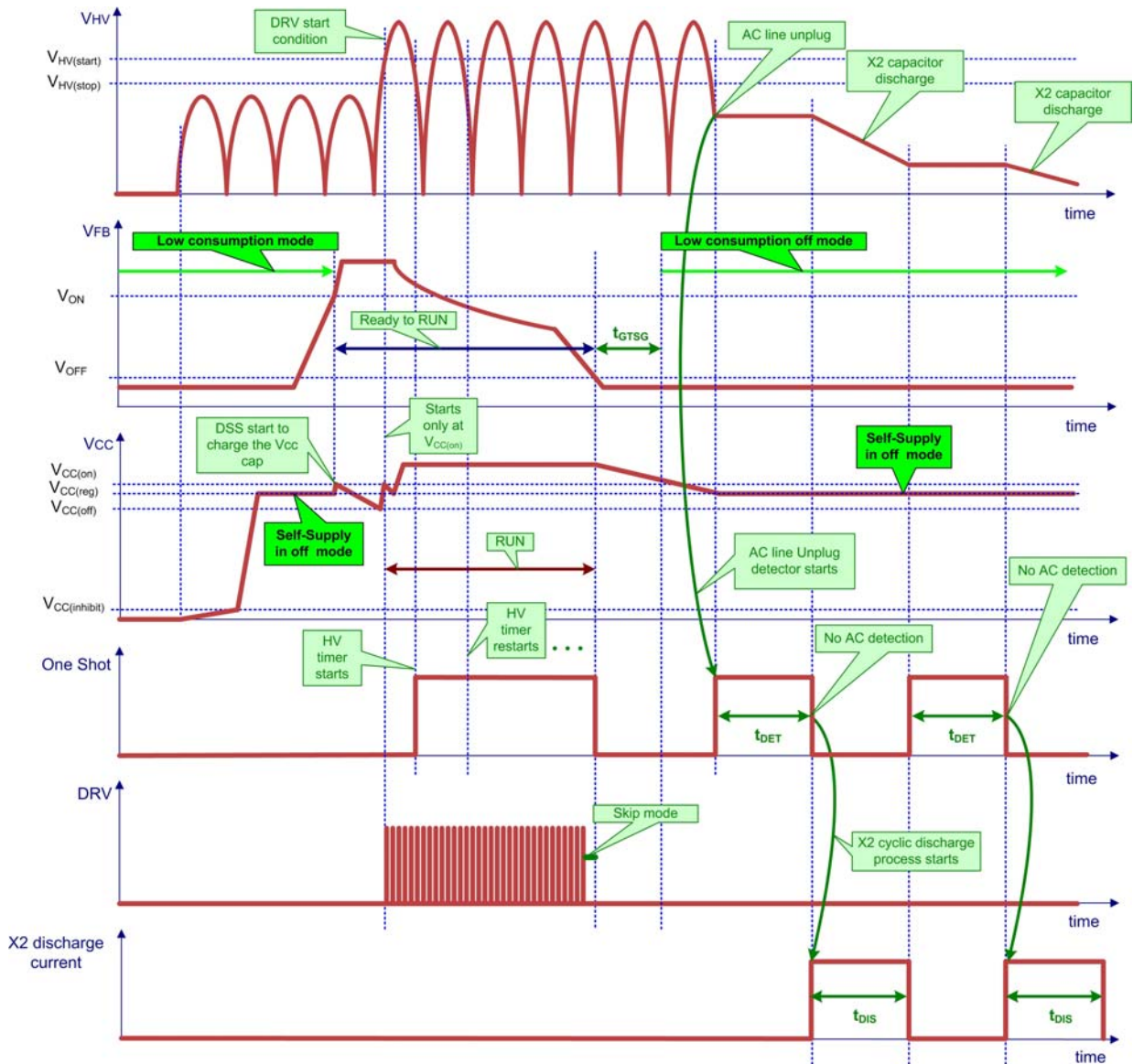


Figure 51. Start-up, Shutdown and AC Line Unplug Time Diagram

**Oscillator with Maximum On Time and Frequency Jittering**

The SCY99194 includes an oscillator that sets the switching frequency 65 kHz. The maximum duty cycle is 80%. In order to improve the EMI signature, the switching frequency jitters  $\pm 6\%$  around its nominal value, with a triangle-wave shape and at a frequency of 125 Hz. This frequency jittering is active even when the frequency is decreased to improve the efficiency in light load condition.

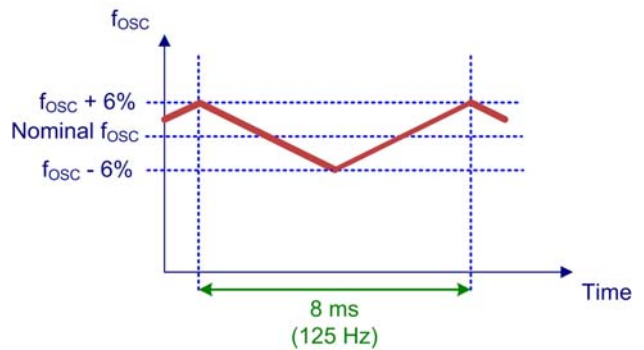


Figure 52. Frequency Modulation of the Maximum Switching Frequency

**Low Load Operation Modes: Frequency Foldback Mode (FFM) and Skip Mode**

In order to improve the efficiency in light load conditions, the frequency of the internal oscillator is linearly reduced from its nominal value down to  $f_{OSC(min)}$ . This frequency foldback starts when the voltage on FB pin goes below  $V_{FB(foldS)}$ , and is complete when  $V_{FB}$  reaches  $V_{FB(foldE)}$ . The maximum on-time duration control is kept during the

frequency foldback mode to provide the natural transformer core anti-saturation protection. The frequency jittering is still active while the oscillator frequency decreases as well. The current setpoint is fixed to 300 mV in the frequency foldback mode if the feedback voltage decreases below the  $V_{FB(freeze)}$  level. This feature increases efficiency under the light loads conditions as well.

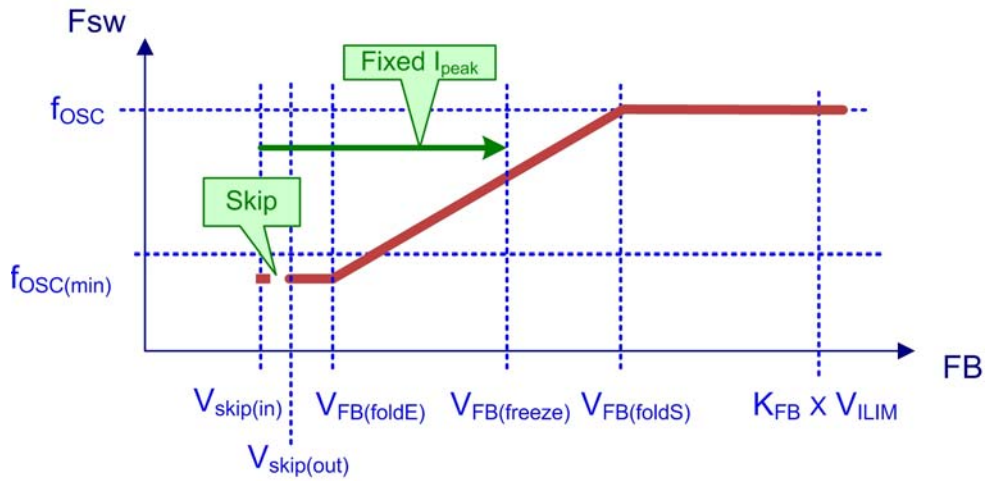


Figure 53. Frequency Foldback Mode Characteristic

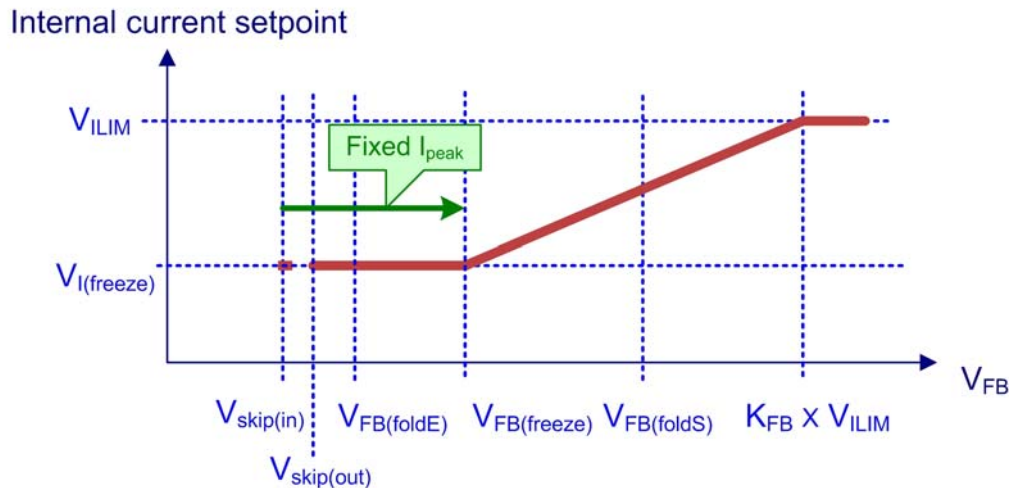


Figure 54. Current Setpoint Dependency on the Feedback Pin Voltage

When the FB voltage reaches  $V_{skip(in)}$  while decreasing, skip mode is activated: the driver stops, and the internal consumption of the controller is decreased. While  $V_{FB}$  is

below  $V_{skip(out)}$ , the controller remains in this state; but as soon as  $V_{FB}$  crosses the skip out threshold, the DRV pin starts to pulse again.

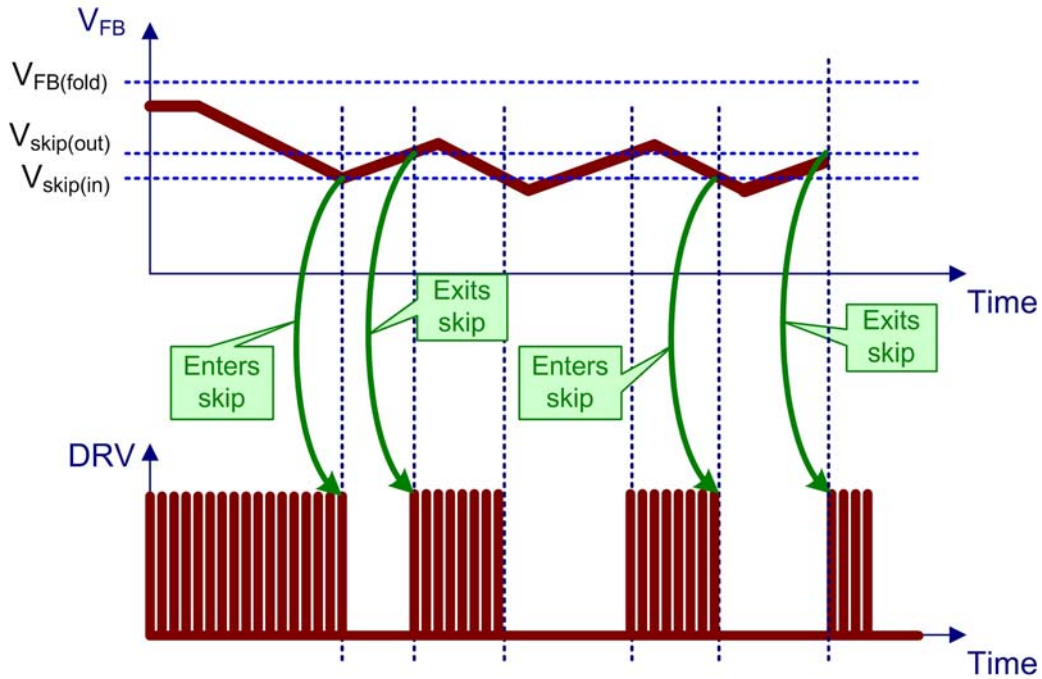


Figure 55. Skip Mode Timing Diagram

**Clamped Driver**

The supply voltage for the SCY99194 can be as high as 28 V, but most of the MOSFETs that will be connected to the DRV pin cannot accept more than 20 V on their gate. The driver pin is therefore clamped safely below 16 V. This driver has a typical capability of 500 mA for source current and 800 mA for sink current.

**Current-Mode Control With Slope Compensation and Soft-Start**

SCY99194 is a current-mode controller, which means that the FB voltage sets the peak current flowing in the inductance and the MOSFET. This is done through a PWM comparator: the current is sensed across a resistor and the

resulting voltage is applied to the CS pin. It is applied to one input of the PWM comparator through a 250 ns LEB block. On the other input the FB voltage divided by 5 sets the threshold: when the voltage ramp reaches this threshold, the output driver is turned off. The maximum value for the current sense is 0.7 V, and it is set by a dedicated comparator.

Each time the controller is starting, i.e. the controller was off and starts – or restarts – when  $V_{CC}$  reaches  $V_{CC(on)}$ , a soft-start is applied: the current sense setpoint is increased by 15 discrete steps from 0 (the minimum level can be higher than 0 because of the LEB and propagation delay) until it reaches  $V_{ILIM}$  (after a duration of  $t_{SSTART}$ ), or until the FB loop imposes a setpoint lower than the one imposed by the soft-start (the two comparators outputs are OR'ed).

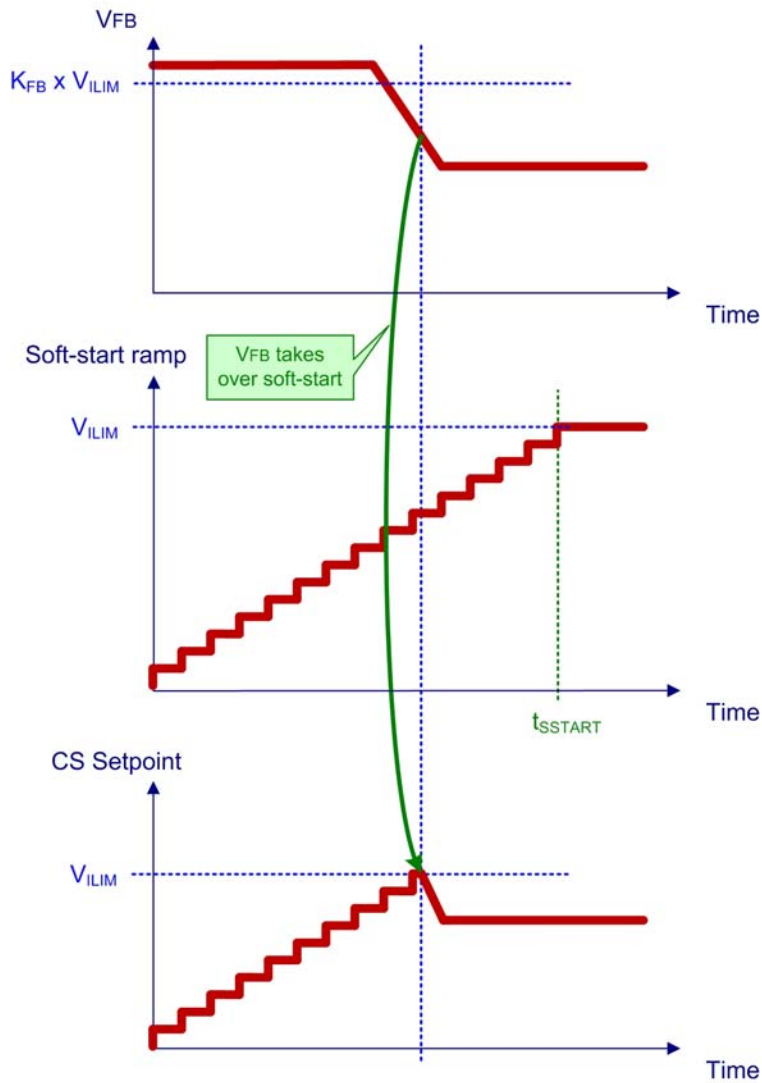


Figure 56. Soft-Start Feature

Under some conditions, like a winding short-circuit for instance, not all the energy stored during the *on* time is transferred to the output during the *off* time, even if the on time duration is at its minimum (imposed by the propagation delay of the detector added to the LEB duration). As a result, the current sense voltage keeps on increasing above  $V_{ILIM}$ , because the controller is blind during the LEB blanking time. Dangerously high current can grow in the system if nothing is done to stop the controller. That's what the additional comparator, that senses when the current sense voltage on CS pin reaches  $V_{CS(stop)} (= 1.5 \times V_{ILIM})$ , does: as soon as this comparator toggles, the controller immediately enters the protection mode.

In order to allow the SCY99194 to operate in CCM with a duty cycle above 50%, the fixed slope compensation is internally applied to the current-mode control. The slope appearing on the internal voltage setpoint for the PWM comparator is  $-32.5 \text{ mV}/\mu\text{s}$  typical for the 65 kHz version. The slope compensation can be observable as a value of the peak current at CS pin.

The internal slope compensation circuitry uses a sawtooth signal synchronized with the internal oscillator is subtracted from the FB voltage divided by  $K_{FB}$ .

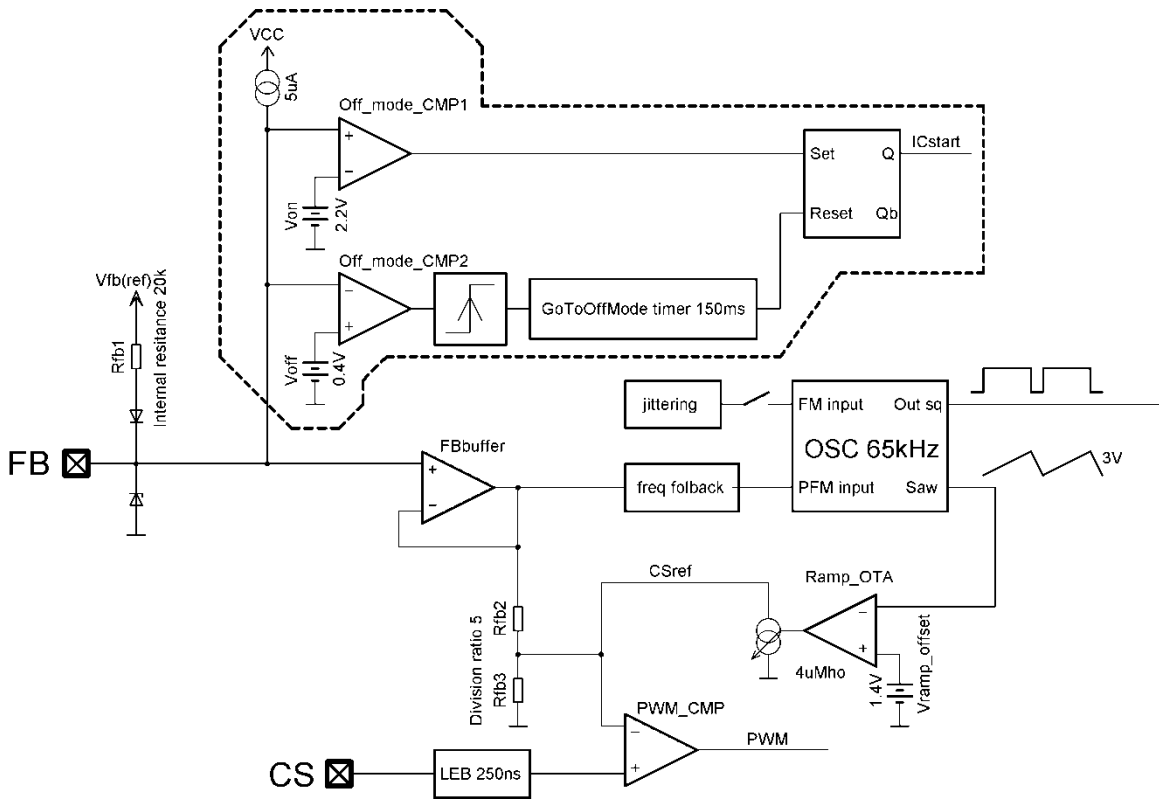


Figure 57. Slope Compensation Block Diagram

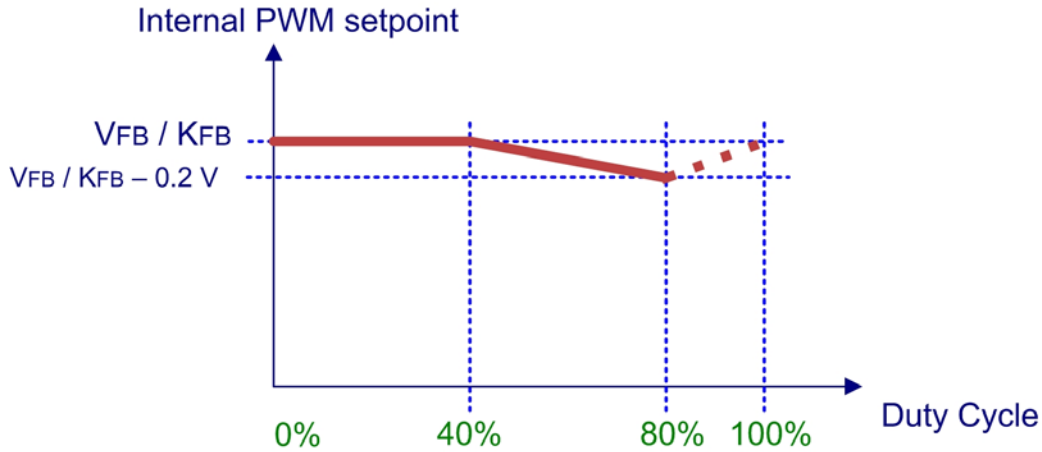


Figure 58. Slope Compensation Timing Diagram

**Internal Overpower Protection**

The power delivered by a flyback power supply is proportional to the square of the peak current in discontinuous conduction mode:

$$P_{OUT} = \frac{1}{2} \cdot \eta \cdot L_P \cdot F_{SW} \cdot I_P^2 \quad (\text{eq. 3})$$

Unfortunately, due to the inherent propagation delay of the logic, the actual peak current is higher at high input voltage than at low input voltage, leading to a significant difference in the maximum output power delivered by the power supply.

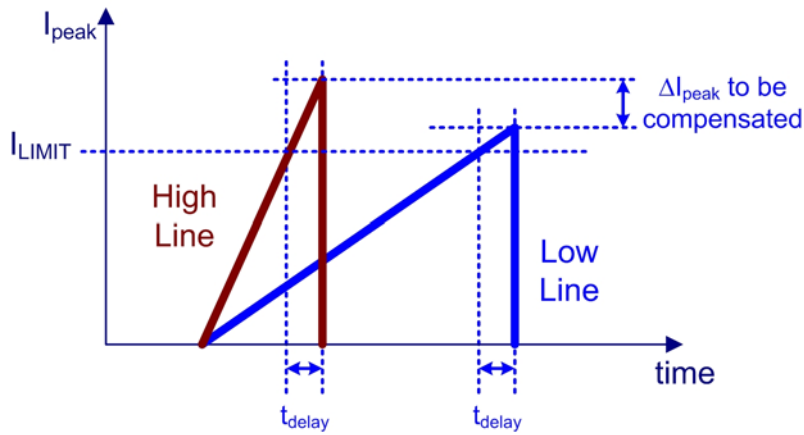


Figure 59. Needs for Line Compensation For True Overpower Protection

To compensate this and have an accurate overpower protection, an offset proportional to the input voltage is added on the CS signal by turning on an internal current source: by adding an external resistor in series between the sense resistor and the CS pin, a voltage offset is created across it by the current. The compensation can be adjusted by changing the value of the resistor.

But this offset is unwanted to appear when the current sense signal is small, i.e. in light load conditions, where it

would be in the same order of magnitude. Therefore the compensation current is only added when the FB voltage is higher than  $V_{FB(OPCE)}$ . However, because the HV pin can be connected to an ac voltage, there is needed an additional circuitry to read or at least closely estimate the actual voltage on the bulk capacitor.

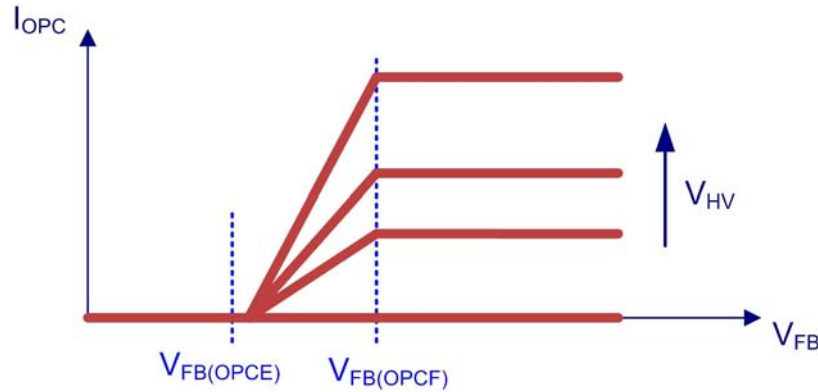


Figure 60. Overpower Protection Current Relation to Feedback Voltage

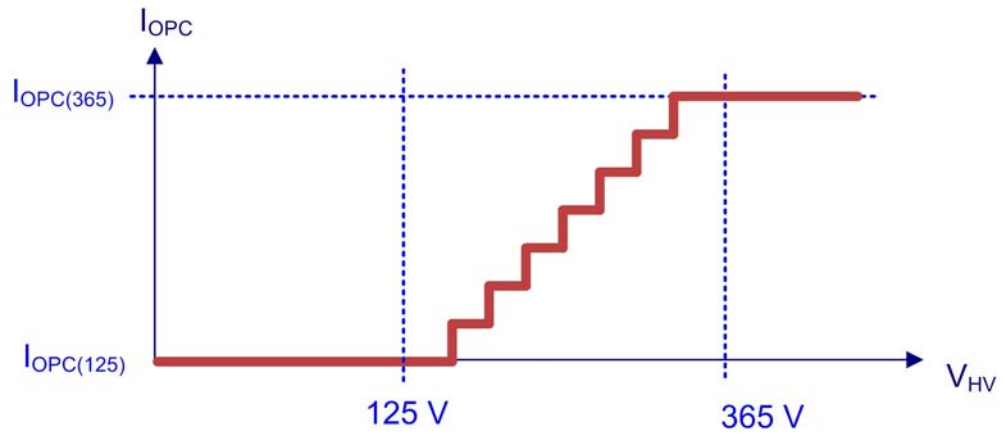


Figure 61. Overpower Protection Current Relation to Peak of Rectified Input Line AC voltage

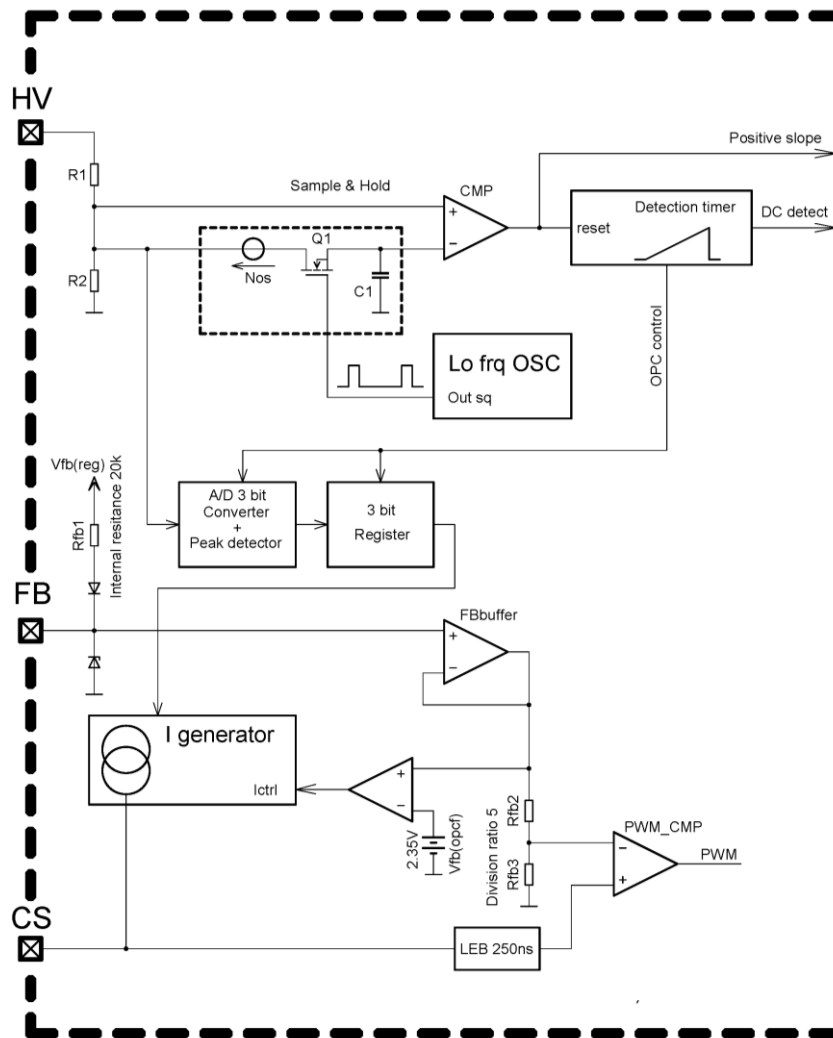


Figure 62. Block Schematic of Overpower Protection Circuit



A 3 bit A/D converter with the peak detector senses the ac input, and its output is periodically sampled and reset, in order to follow closely the input voltage variations. The sample and reset events are given by the output from the ac line unplug detector. The sensed HV pin voltage peak value is validated when no HV edges from comparator are present after last falling edge during two sample clocks. See Figure 63 for details.

### Overcurrent Protection with Fault timer

The overload protection depends only on the current sensing signal, making it able to work with any transformer, even with very poor coupling or high leakage inductance.

When an overcurrent occurs on the output of the power supply, the FB loop asks for more power than the controller can deliver, and the CS setpoint reaches  $V_{ILIM}$ . When this event occurs, an internal  $t_{fault}$  timer is started: once the timer

times out, DRV pulses are stopped and the controller is either latched off (latched protection, option A) or this latch can be released in autorecovery mode (option B), the controller tries to restart after  $t_{autorec}$ . Another possibility of the latch release is the  $V_{CC}$  power on reset or the ac line unplug event detected via ac detector. Therefore the latch can be released by the end of the 1<sup>st</sup> X2 discharge event. The timer is reset when the CS setpoint goes back below  $V_{ILIM}$  before the timer elapses. The fault timer is also started if the driver signal is reset by the max duty-ratio. The controller also enters the same protection mode if the voltage on the CS pin reaches 1.5 times the maximum internal setpoint  $V_{CS(stop)}$  (allows to detect winding short-circuits) or there appears low  $V_{CC}$  supply. See Figures 64 and 65 for the timing diagram.

In autorecovery mode if the fault has gone, the supply resumes operation; if not, the system starts a new burst cycle.

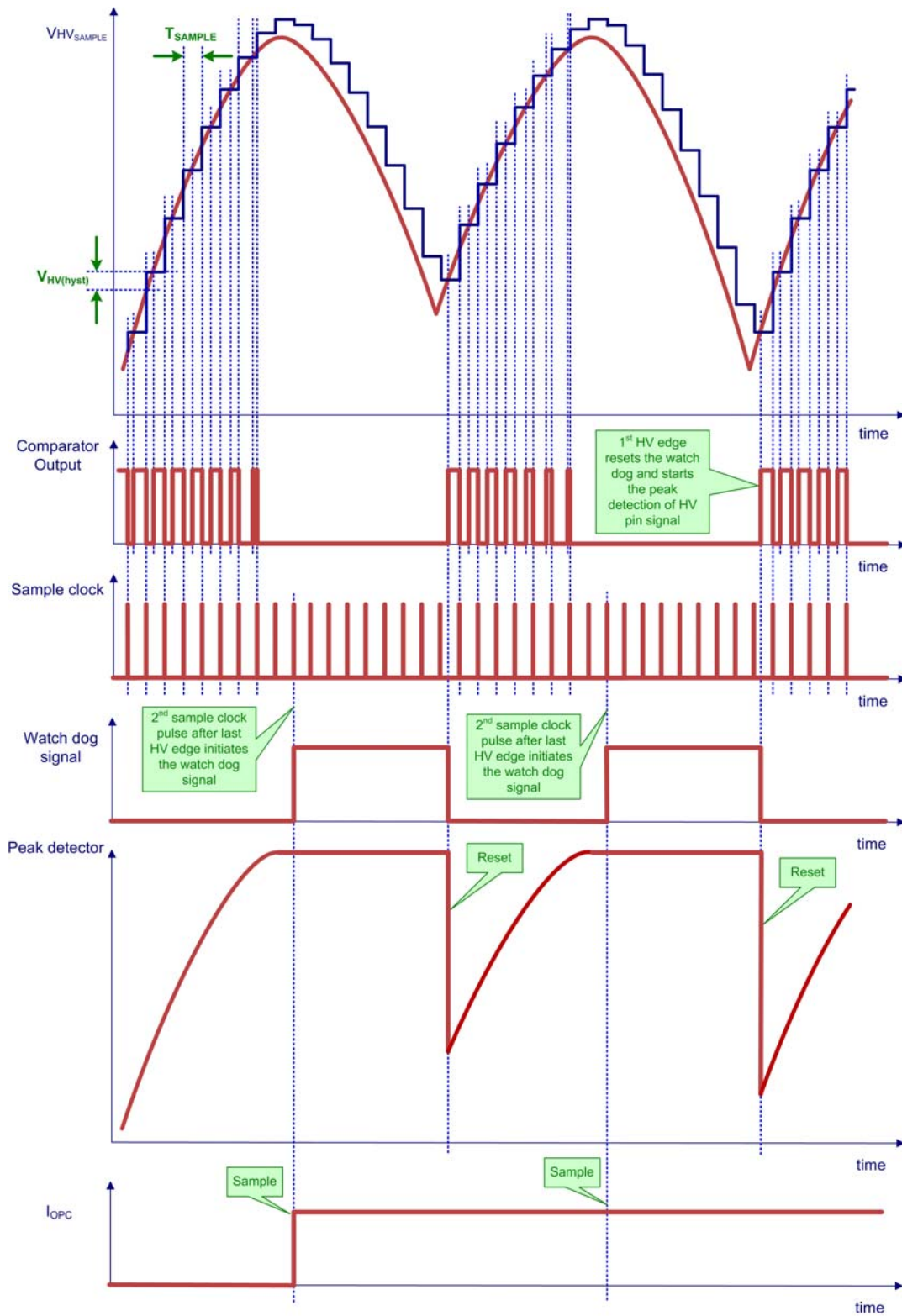


Figure 63. Overpower Compensation Timing Diagram

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## PROTECTION MODES AND THE LATCH MODE RELEASES

Event	Timer Protection	Next Device Status	Release to Normal Operation Mode
Overcurrent $V_{ILIM} > 0.7\text{ V}$	Fault timer	Latch	Autorecovery – B version 1 <sup>st</sup> X2 discharge event $V_{CC} < V_{CC(reset)}$
Winding short $V_{sense} > V_{CS(stop)}$	Immediate reaction	Latch	Autorecovery – B version 1 <sup>st</sup> X2 discharge event $V_{CC} < V_{CC(reset)}$
Low supply $V_{CC} < V_{CC(off)}$	10 $\mu\text{s}$ timer	Latch	1 <sup>st</sup> X2 discharge event $V_{CC} \geq V_{CC(reset)}$
External OTP, OVP	55 $\mu\text{s}$	Latch	1 <sup>st</sup> X2 discharge event $V_{CC} < V_{CC(on)}$
High supply $V_{CC} > V_{CC(ovp)}$	10 $\mu\text{s}$ timer	Latch	1 <sup>st</sup> X2 discharge event $V_{CC} < V_{CC(reset)}$
Internal TSD	10 $\mu\text{s}$ timer	Device stops, HV start-up current source stops	$(V_{CC} > V_{CC(on)})$ & TSDb
Off mode $V_{FB} < V_{OFF}$	600 ms timer	Device stops and internal $V_{CC}$ is turned off	$(V_{CC} > V_{CC(on)})$ & $(V_{FB} > V_{ON})$

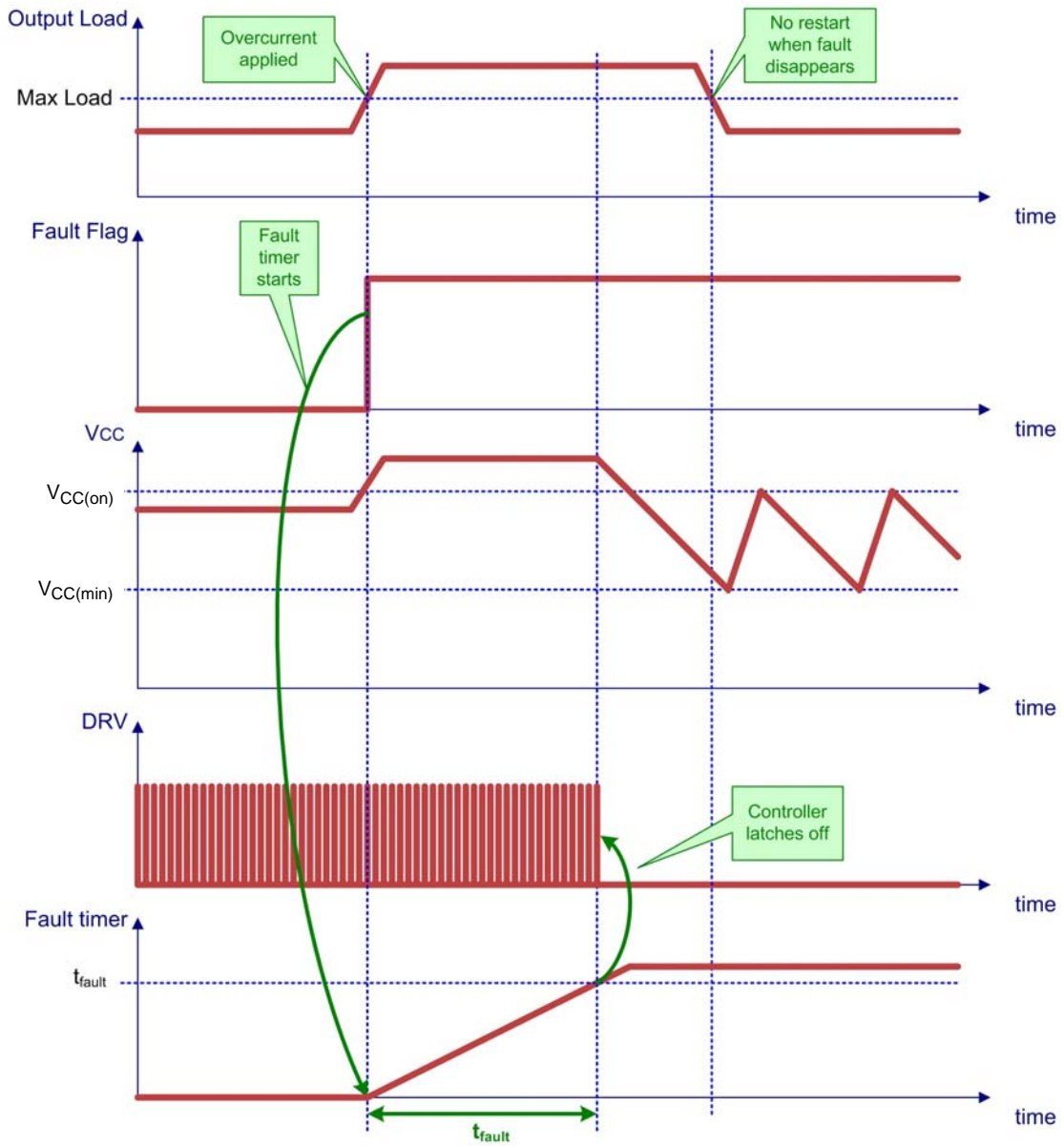


Figure 64. Latched Timer-Based Overcurrent Protection (Option A)

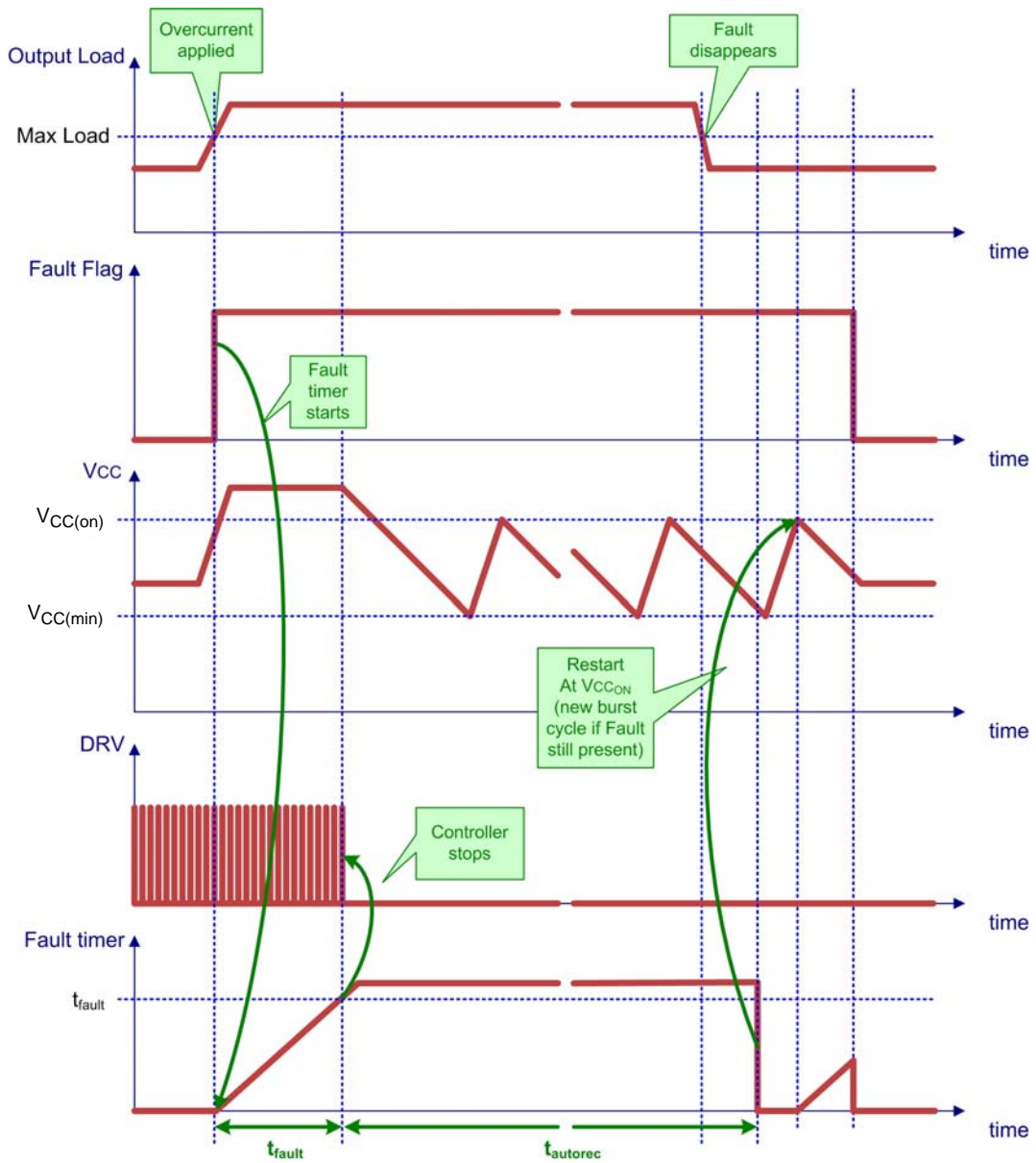


Figure 65. Timer-Based Protection Mode with Autorecovery Release from Latch-off (Option B)

Latch-Off Input

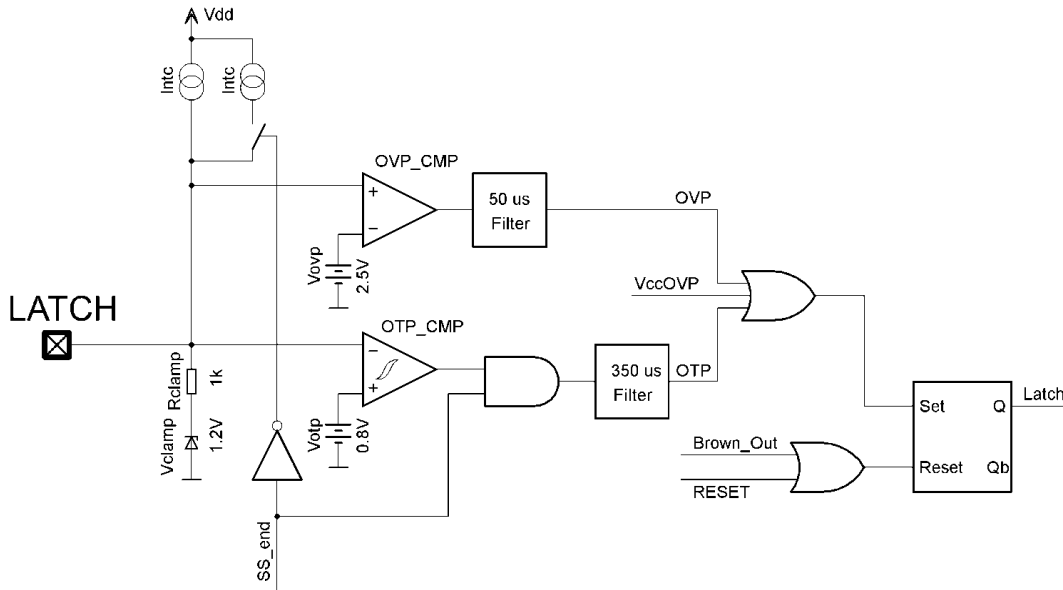


Figure 66. Latch Detection Schematic

The Latch pin is dedicated to the latch-off function: it includes two levels of detection that define a working window, between a high latch and a low latch: within these two thresholds, the controller is allowed to run, but as soon as either the low or the high threshold is crossed, the controller is latched off. The lower threshold is intended to be used with an NTC thermistor, thanks to an internal current source  $I_{NTC}$ .

An active clamp prevents the voltage from reaching the high threshold if it is only pulled up by the  $I_{NTC}$  current. To reach the high threshold, the pull-up current has to be higher than the pull-down capability of the clamp (typically 1.5 mA at  $V_{OVP}$ ).

To avoid any false triggering, spikes shorter than 50  $\mu$ s or 350  $\mu$ s (for the low latch) are blanked and only longer signals can actually latch the controller.

Reset occurs the  $V_{CC}$  is cycled down to a reset voltage, which in a real application can only happen if the power supply is unplugged from the ac line.

Upon startup, the internal references take some time before being at their nominal values; so one of the comparators could toggle even if it should not. Therefore the internal logic does not take the latch signal into account before the controller is ready to start: once  $V_{CC}$  reaches  $V_{CC(on)}$ , the latch pin High latch state is taken into account and the DRV switching starts only if it is allowed; whereas the Low latch (typically sensing an over temperature) is taken into account only after the soft-start is finished. In addition, the NTC current is doubled to  $I_{NTC(SSTART)}$  during the soft-start period, to speed up the charging of the Latch pin capacitor. The maximum value of Latch pin capacitor is given by the following formula (The standard start-up condition is considered and the NTC current is neglected):

$$C_{LATCH \max} = \frac{t_{SSTART \min} \cdot I_{NTC(SSTART) \min}}{V_{clamp0 \min}} = \frac{8.0 \cdot 10^{-3} \cdot 130 \cdot 10^{-6}}{1.0} \text{ F} = 1.04 \mu\text{F} \quad (\text{eq. 4})$$

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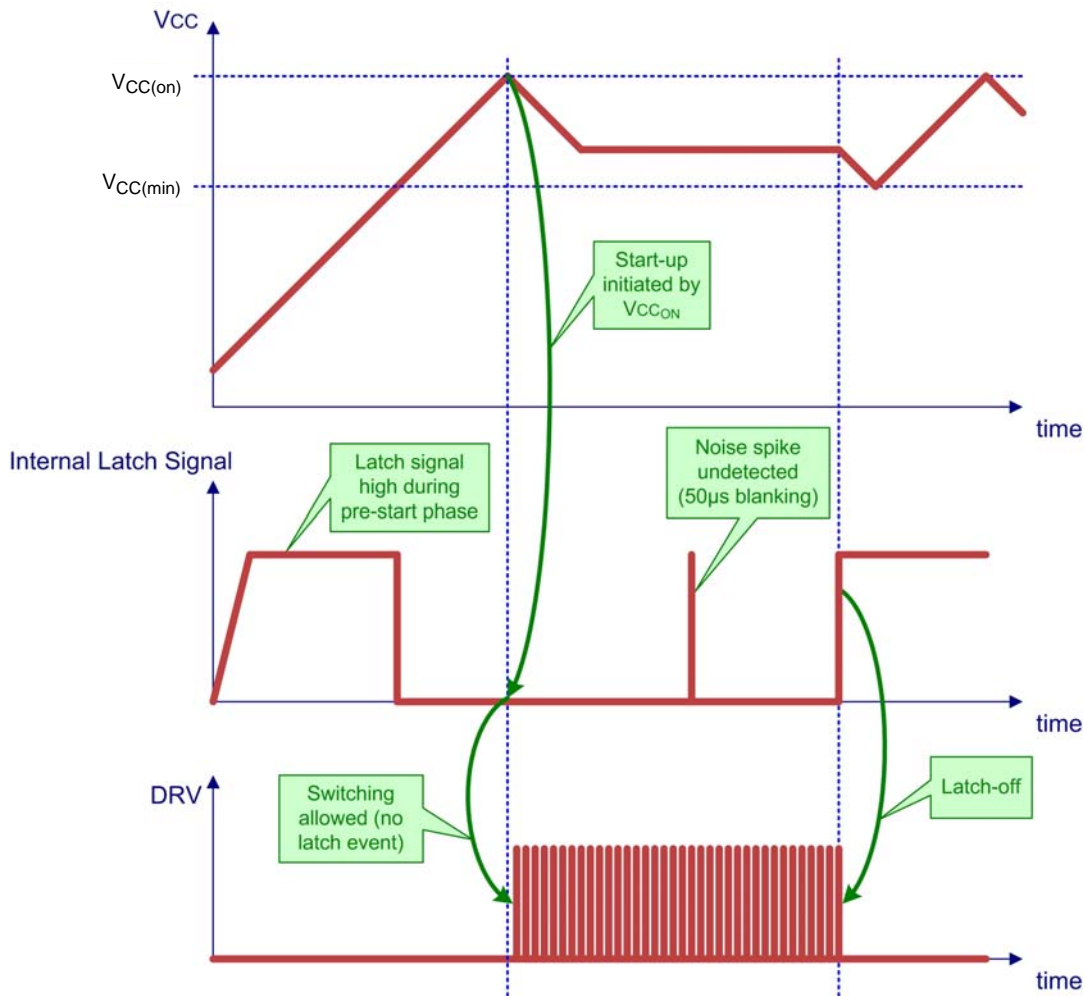


Figure 67. Latch Timing Diagram

## Temperature Shutdown

The SCY99194 includes a temperature shutdown protection with a trip point typically at 150°C and the typical hysteresis of 30°C. When the temperature rises above the high threshold, the controller stops switching instantaneously, and goes to the off mode with extremely

low power consumption. There is kept the VCC supply to keep the TSD information. When the temperature falls below the low threshold, the start-up of the device is enabled again, and a regular start-up sequence takes place. See the status diagrams at the Figures 41 and 42.

## ORDERING INFORMATION 5

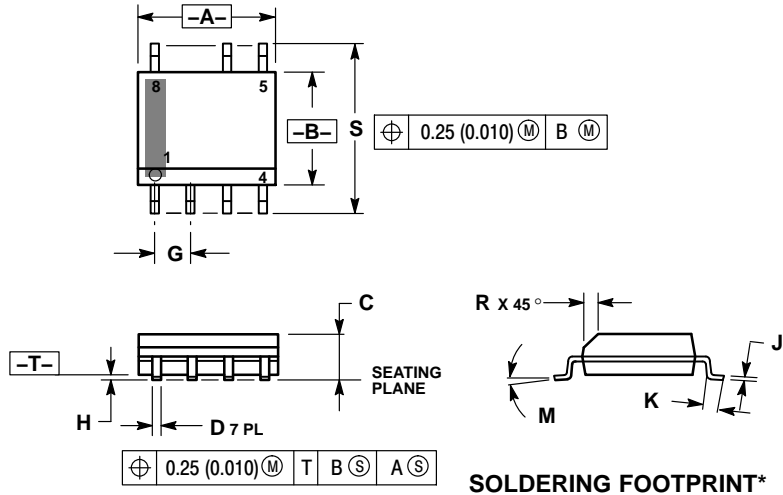
Delta Device Part No.	ON Semiconductor Ordering Part No.	Marking	Overload Protection	Switching Frequency	Package	Shipping†
DAP041	SCY99194AD065R2G	DAP041	Latched	65 kHz	SOIC-7 (Pb-Free)	2500 / Tape & Reel

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

# SCY99194

## PACKAGE DIMENSIONS

### SOIC-7 CASE 751U ISSUE E

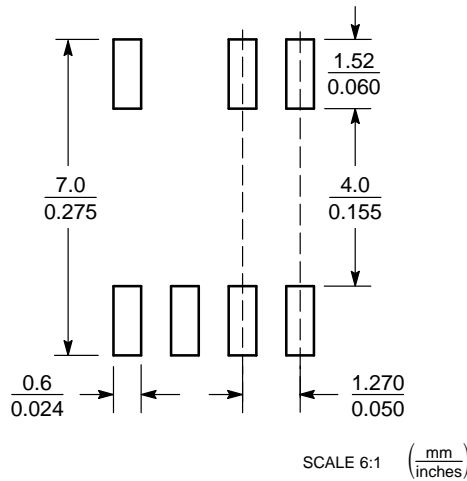


#### NOTES:

1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: MILLIMETER.
3. DIMENSION A AND B ARE DATUMS AND T IS A DATUM SURFACE.
4. DIMENSION A AND B DO NOT INCLUDE MOLD PROTRUSION.
5. MAXIMUM MOLD PROTRUSION 0.15 (0.006) PER SIDE.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	4.80	5.00	0.189	0.197
B	3.80	4.00	0.150	0.157
C	1.35	1.75	0.053	0.069
D	0.33	0.51	0.013	0.020
G	1.27 BSC		0.050 BSC	
H	0.10	0.25	0.004	0.010
J	0.19	0.25	0.007	0.010
K	0.40	1.27	0.016	0.050
M	0°	8°	0°	8°
N	0.25	0.50	0.010	0.020
S	5.80	6.20	0.228	0.244

#### SOLDERING FOOTPRINT\*



\*For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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